

8-114 Steam expands in a two-stage adiabatic turbine from a specified state to another specified state. Steam is reheated between the stages. For a given power output, the reversible power output and the rate of exergy destruction are to be determined.

Assumptions 1 This is a steady-flow process since there is no change with time. **2** Kinetic and potential energy changes are negligible. **3** The turbine is adiabatic and thus heat transfer is negligible. **4** The environment temperature is given to be $T_0 = 25^\circ\text{C}$.

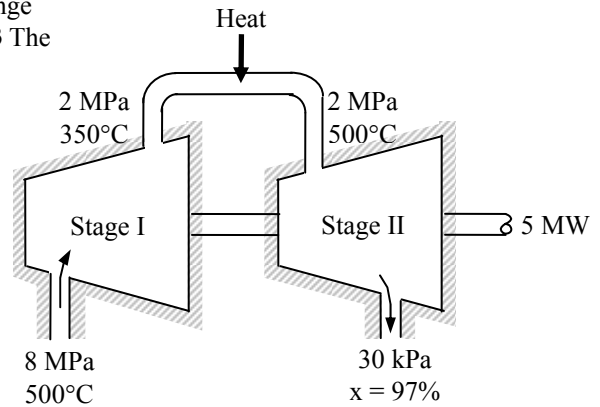
Properties From the steam tables (Tables A-4 through 6)

$$\left. \begin{array}{l} P_1 = 8 \text{ MPa} \\ T_1 = 500^\circ\text{C} \end{array} \right\} \begin{array}{l} h_1 = 3399.5 \text{ kJ/kg} \\ s_1 = 6.7266 \text{ kJ/kg}\cdot\text{K} \end{array}$$

$$\left. \begin{array}{l} P_2 = 2 \text{ MPa} \\ T_2 = 350^\circ\text{C} \end{array} \right\} \begin{array}{l} h_2 = 3137.7 \text{ kJ/kg} \\ s_2 = 6.9583 \text{ kJ/kg}\cdot\text{K} \end{array}$$

$$\left. \begin{array}{l} P_3 = 2 \text{ MPa} \\ T_3 = 500^\circ\text{C} \end{array} \right\} \begin{array}{l} h_3 = 3468.3 \text{ kJ/kg} \\ s_3 = 7.4337 \text{ kJ/kg}\cdot\text{K} \end{array}$$

$$\left. \begin{array}{l} P_4 = 30 \text{ kPa} \\ x_4 = 0.97 \end{array} \right\} \begin{array}{l} h_4 = h_f + x_4 h_{fg} = 289.27 + 0.97 \times 2335.3 = 2554.5 \text{ kJ/kg} \\ s_4 = s_f + x_4 s_{fg} = 0.9441 + 0.97 \times 6.8234 = 7.5628 \text{ kJ/kg}\cdot\text{K} \end{array}$$



Analysis We take the entire turbine, excluding the reheat section, as the system, which is a control volume. The energy balance for this steady-flow system can be expressed in the rate form as

$$\underbrace{\dot{E}_{\text{in}} - \dot{E}_{\text{out}}}_{\text{Rate of net energy transfer by heat, work, and mass}} = \underbrace{\Delta \dot{E}_{\text{system}}^{\text{0}}}_{\text{Rate of change in internal, kinetic, potential, etc. energies}} \stackrel{\text{0 (steady)}}{=} 0$$

$$\dot{E}_{\text{in}} = \dot{E}_{\text{out}}$$

$$\dot{m}h_1 + \dot{m}h_3 = \dot{m}h_2 + \dot{m}h_4 + \dot{W}_{\text{out}}$$

$$\dot{W}_{\text{out}} = \dot{m}[(h_1 - h_2) + (h_3 - h_4)]$$

Substituting, the mass flow rate of the steam is determined from the steady-flow energy equation applied to the actual process,

$$\dot{m} = \frac{\dot{W}_{\text{out}}}{h_1 - h_2 + h_3 - h_4} = \frac{5000 \text{ kJ/s}}{(3399.5 - 3137.7 + 3468.3 - 2554.5) \text{ kJ/kg}} = 4.253 \text{ kg/s}$$

The reversible (or maximum) power output is determined from the rate form of the exergy balance applied on the turbine and setting the exergy destruction term equal to zero,

$$\underbrace{\dot{X}_{\text{in}} - \dot{X}_{\text{out}}}_{\text{Rate of net exergy transfer by heat, work, and mass}} - \underbrace{\dot{X}_{\text{destroyed}}^{\text{0}}}_{\text{Rate of exergy destruction}} \stackrel{\text{0 (reversible)}}{=} \underbrace{\Delta \dot{X}_{\text{system}}^{\text{0}}}_{\text{Rate of change of exergy}} \stackrel{\text{0 (steady)}}{=} 0$$

$$\dot{X}_{\text{in}} = \dot{X}_{\text{out}}$$

$$\dot{m}\psi_1 + \dot{m}\psi_3 = \dot{m}\psi_2 + \dot{m}\psi_4 + \dot{W}_{\text{rev,out}}$$

$$\begin{aligned} \dot{W}_{\text{rev,out}} &= \dot{m}(\psi_1 - \psi_2) + \dot{m}(\psi_3 - \psi_4) \\ &= \dot{m}[(h_1 - h_2) + T_0(s_2 - s_1) - \Delta ke^{\text{0}} - \Delta pe^{\text{0}}] \\ &\quad + \dot{m}[(h_3 - h_4) + T_0(s_4 - s_3) - \Delta ke^{\text{0}} - \Delta pe^{\text{0}}] \end{aligned}$$

Then the reversible power becomes

$$\begin{aligned} \dot{W}_{\text{rev,out}} &= \dot{m}[h_1 - h_2 + h_3 - h_4 + T_0(s_2 - s_1 + s_4 - s_3)] \\ &= (4.253 \text{ kg/s})[(3399.5 - 3137.7 + 3468.3 - 2554.5) \text{ kJ/kg} \\ &\quad + (298 \text{ K})(6.9583 - 6.7266 + 7.5628 - 7.4337) \text{ kJ/kg}\cdot\text{K}] \\ &= \mathbf{5457 \text{ kW}} \end{aligned}$$

Then the rate of exergy destruction is determined from its definition,

$$\dot{X}_{\text{destroyed}} = \dot{W}_{\text{rev,out}} - \dot{W}_{\text{out}} = 5457 - 5000 = \mathbf{457 \text{ kW}}$$