

**9-58** A diesel engine with air as the working fluid has a compression ratio of 20. The thermal efficiency and the mean effective pressure are to be determined.

**Assumptions 1** The air-standard assumptions are applicable. **2** Kinetic and potential energy changes are negligible. **3** Air is an ideal gas with constant specific heats.

**Properties** The properties of air at room temperature are  $c_p = 1.005 \text{ kJ/kg}\cdot\text{K}$ ,  $c_v = 0.718 \text{ kJ/kg}\cdot\text{K}$ ,  $R = 0.287 \text{ kJ/kg}\cdot\text{K}$ , and  $k = 1.4$  (Table A-2).

**Analysis** (a) Process 1-2: isentropic compression.

$$T_2 = T_1 \left( \frac{v_1}{v_2} \right)^{k-1} = (293 \text{ K})(20)^{0.4} = 971.1 \text{ K}$$

Process 2-3:  $P = \text{constant}$  heat addition.

$$\frac{P_3 v_3}{T_3} = \frac{P_2 v_2}{T_2} \longrightarrow \frac{v_3}{v_2} = \frac{T_3}{T_2} = \frac{2200 \text{ K}}{971.1 \text{ K}} = 2.265$$

Process 3-4: polytropic expansion.

$$T_4 = T_3 \left( \frac{v_3}{v_4} \right)^{n-1} = T_3 \left( \frac{2.265 v_2}{v_4} \right)^{n-1} = T_3 \left( \frac{2.265}{r} \right)^{n-1} = (2200 \text{ K}) \left( \frac{2.265}{20} \right)^{0.35} = 1026 \text{ K}$$

$$q_{\text{in}} = h_3 - h_2 = c_p (T_3 - T_2) = (1.005 \text{ kJ/kg}\cdot\text{K})(2200 - 971.1) \text{ K} = 1235 \text{ kJ/kg}$$

$$q_{\text{out}} = u_4 - u_1 = c_v (T_4 - T_1) = (0.718 \text{ kJ/kg}\cdot\text{K})(1026 - 293) \text{ K} = 526.3 \text{ kJ/kg}$$

Note that  $q_{\text{out}}$  in this case does not represent the entire heat rejected since some heat is also rejected during the polytropic process, which is determined from an energy balance on process 3-4:

$$w_{34,\text{out}} = \frac{R(T_4 - T_3)}{1 - n} = \frac{(0.287 \text{ kJ/kg}\cdot\text{K})(1026 - 2200) \text{ K}}{1 - 1.35} = 963 \text{ kJ/kg}$$

$$E_{\text{in}} - E_{\text{out}} = \Delta E_{\text{system}}$$

$$\begin{aligned} q_{34,\text{in}} - w_{34,\text{out}} &= u_4 - u_3 \longrightarrow q_{34,\text{in}} = w_{34,\text{out}} + c_v (T_4 - T_3) \\ &= 963 \text{ kJ/kg} + (0.718 \text{ kJ/kg}\cdot\text{K})(1026 - 2200) \text{ K} \\ &= 120.1 \text{ kJ/kg} \end{aligned}$$

which means that 120.1 kJ/kg of heat is transferred to the combustion gases during the expansion process. This is unrealistic since the gas is at a much higher temperature than the surroundings, and a hot gas loses heat during polytropic expansion. The cause of this unrealistic result is the constant specific heat assumption. If we were to use  $u$  data from the air table, we would obtain

$$q_{34,\text{in}} = w_{34,\text{out}} + (u_4 - u_3) = 963 + (781.3 - 1872.4) = -128.1 \text{ kJ/kg}$$

which is a heat loss as expected. Then  $q_{\text{out}}$  becomes

$$q_{\text{out}} = q_{34,\text{out}} + q_{41,\text{out}} = 128.1 + 526.3 = 654.4 \text{ kJ/kg}$$

and

$$w_{\text{net,out}} = q_{\text{in}} - q_{\text{out}} = 1235 - 654.4 = 580.6 \text{ kJ/kg}$$

$$\eta_{\text{th}} = \frac{w_{\text{net,out}}}{q_{\text{in}}} = \frac{580.6 \text{ kJ/kg}}{1235 \text{ kJ/kg}} = \mathbf{47.0\%}$$

$$(b) \quad v_1 = \frac{RT_1}{P_1} = \frac{(0.287 \text{ kPa}\cdot\text{m}^3/\text{kg}\cdot\text{K})(293 \text{ K})}{95 \text{ kPa}} = 0.885 \text{ m}^3/\text{kg} = v_{\text{max}}$$

$$v_{\text{min}} = v_2 = \frac{v_{\text{max}}}{r}$$

$$\text{MEP} = \frac{w_{\text{net,out}}}{v_1 - v_2} = \frac{w_{\text{net,out}}}{v_1(1 - 1/r)} = \frac{580.6 \text{ kJ/kg}}{(0.885 \text{ m}^3/\text{kg})(1 - 1/20)} \left( \frac{1 \text{ kPa}\cdot\text{m}^3}{\text{kJ}} \right) = \mathbf{691 \text{ kPa}}$$

