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Conclusions

Immersed boundary simulations of gravitational settling

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MIT Conference on Computational Fluid and Solid Mechanics

June 12, 2013

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Acknowledgments

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Natural Sciences and Engineering Research Council of Canada

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Motivation: Sedimentation in applications

Sedimentation is the settling of particles under the influence of gravity:

- Biofilm dynamics.
- Marine organisms: algae, jellyfish.
- Industrial processes: wood pulp fibers, crystal precipitation, mine tailings.
- Natural phenomena: hailstorms, sediment transport in rivers and lakes.
- Tea leaves in a teacup.





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Previous work on sedimentation

Gravitational settling of particle suspensions has been studied extensively in the literature using

- mathematical analysis,
- experiments,
- numerical simulations.

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Analytical solutions

• Stokes' law (1851): in a creeping flow of infinite extent, balancing gravity and drag forces yields settling velocity for a sphere in 3D:

$$V_s = \frac{gD^2(\rho_p - \rho_f)}{18\mu}$$

where D = diameter, $\mu =$ viscosity.

- Analogous result can be derived for a 2D circular particle (infinite cylinder) ⇒ a nonlinear equation in V_s.
- An overview of more recent analytical results can be found in Guazzelli & Morris (2012).



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Experimental results

- An enormous experimental literature exists owing to the importance of sedimentation in industrial and other applications. [Davis & Acrivos, 1985]
- Of particular interest to us are estimates of wall-corrected settling velocity for a particle in a channel of width *W*:

$$\widetilde{V}_s = rac{V_s}{\lambda(k)}$$
 where $k = rac{D}{W}$

and $\lambda(k)$ is a fitted correction factor.

• For example, Faxén's (1946) experiments yield

$$\lambda(k) pprox rac{-4\pi}{0.9157 + \ln(k) - 1.724k^2 + 1.730k^4 - 2.406k^6 + 4.591k^8}$$

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- Many authors have simulated 2D and 3D suspension flows numerically using:
 - finite element method,
 - lattice-Boltzmann method,
 - boundary element method,
 - . . .
- IB method has been applied to gravitational settling of
 - rigid fibers [Wang & Layton, 2009]
 - suspensions of swimming algal cells [Hopkins & Fauci, 2002]
- Direct-forcing IB approach has also been applied to sedimentation [Uhlmann, 2005] [Wang, Fan & Luo, 2008] [Breugem, 2012]
- However, there has not yet been an extensive validation of the IB method for particulate flows with settling.





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 [Hopkins & Fauci, 2002] ← basis for our approach!
- Direct-forcing IB approach has also been applied to sedimentation [Uhlmann, 2005] [Wang, Fan & Luo, 2008] [Breugem, 2012]
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Aims of this study

- Sedimentation is very well-studied for rigid particles such as spheres, ellipsoids, fibers, . . .
- For simplicity, we consider spherical particles that are only slightly heavier than the suspending fluid: $\frac{\rho_p \rho_f}{\rho_c} \ll 1$.
- We develop a very general numerical approach and validate it using results for rigid particles.
- Our long-term aim is to simulate sedimentation of both rigid and deformable particles. Hence, the need for the IB method!

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Problem geometry





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Governing equations

Variables: $\mathbf{u}(\mathbf{x}, t) = \text{velocity}, \ p(\mathbf{x}, t) = \text{pressure}, \ \mathbf{X}(s, t) = \text{IB position}$

Parameters: ρ_f = fluid density, ρ_p = particle density, μ = viscosity

Incompressible Navier-Stokes equations: (Boussinesq approximation, $\rho_p \gtrsim \rho_f$)

$$\rho_f \frac{\partial \mathbf{u}}{\partial t} + \rho_f \mathbf{u} \cdot \nabla \mathbf{u} = \mu \nabla^2 \mathbf{u} - \nabla p + \mathbf{f}_{IB} + \mathbf{f}_G$$
$$\nabla \cdot \mathbf{u} = \mathbf{0}$$

IB evolution equation:

$$\frac{\partial \mathbf{X}}{\partial t} = \int_{\Omega} \mathbf{u}(\mathbf{x}, t) \, \delta(\mathbf{x} - \mathbf{X}(s, t)) \, d\mathbf{x}$$

IB elastic force:

$$\mathbf{f}_{IB}(\mathbf{x},t) = \int_{\Gamma^{w,p}} \mathbf{F}_{IB}(s,t) \,\delta(\mathbf{x} - \mathbf{X}(s,t)) \,ds \qquad \begin{array}{c} \text{(specify discrete} \\ \mathbf{F}_{IB} \text{ later}) \end{array}$$

Gravitational settling term:

$$\mathbf{f}_G(\mathbf{x},t) = -\begin{bmatrix} 0\\g \end{bmatrix} \int_{\Gamma^p} (\rho_p - \rho_f) \, \delta(\mathbf{x} - \mathbf{X}(s,t)) \, ds \text{ for all } s \in \mathbb{R}$$

Immersed boundary method

We apply a straightforward discretization of the IB problem using:

- centered finite differences in space,
- cosine approximation for delta function,
- ADI for diffusion and advection terms,
- explicit treatment of IB force and settling terms,
- split-step projection scheme, with an FFT solve for the pressure Poisson equation.

Details are in Ghosh & JS [arxiv:1304.0804, 2013].

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Discrete IB force for the walls

• The stationary walls are divided into N_w equally-spaced tether points with fixed locations

$$\mathbf{Y}^w_\ell = \left[(L_x \pm W)/2, \ \ell L_y/N_w
ight] \qquad ext{for } \ell = 1, 2, \dots, N_w$$

 Each wall IB point X_l(t) is connected to the corresponding tether point by a stiff spring with force density

$$\mathbf{F}_{\ell}^{w}(t) = \sigma_{w}(\mathbf{Y}_{\ell}^{w} - \mathbf{X}_{\ell}(t))$$

• The force integral approximation involves a length scaling factor:

$$\mathbf{f}_{i,j} = \sum_{\ell=1}^{N_{w}} \mathbf{F}_{\ell}^{w} \, \delta_{h}(\mathbf{x}_{i,j} - \mathbf{X}_{\ell}) \, \frac{L_{y}}{N_{w}}$$

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Discrete IB force for the particle

- "Uniform" triangulation of particle with nodes $X_{\ell}(t)$ for $\ell = 1, 2, ..., N_{p}$.
- Following Alpkvist & Klapper (2007), edges generate spring forces with

$$\begin{split} \mathbf{F}_{\ell}^{p} &= \sigma_{P} \sum_{\substack{m=1\\ \mathbb{I}_{\ell,m} \neq 0}}^{N_{p}} \mathbb{I}_{\ell,m} \frac{\mathbf{d}_{\ell,m}}{d_{\ell,m}} (d_{\ell,m}(0) - d_{\ell,m} \\ \mathbf{d}_{\ell,m}(t) &= \mathbf{X}_{\ell}(t) - \mathbf{X}_{m}(t) \\ d_{\ell,m} &= |\mathbf{d}_{\ell,m}| \\ \mathbb{I}_{\ell,m} &= [0/1 \text{ incidence matrix }] \end{split}$$

• Force integral is scaled by an area factor:

$$\mathbf{f}_{i,j} = \sum_{\ell=1}^{N_p} \mathbf{F}_{\ell}^p \, \delta_h(\mathbf{x}_{i,j} - \mathbf{X}_{\ell}) \underbrace{\frac{\pi D^2}{4N_p}}_{\bigtriangleup \text{ area}}$$

[Hopkins & Fauci, 2002]



Particle triangulation with $N_p = 2015$ nodes.

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For small $\Delta \rho = \rho_p - \rho_f$, the settling velocity V_s approaches Faxén's (1946) result as the channel length L_y increases:



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Single particle: Varying particle size

Wall-corrected \widetilde{V}_s formulas are only valid for small k = W/D.



Our simulations demonstrate physically reasonable behaviour as $k \rightarrow 1$.

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Single particle: Released off-center

- At Reynolds number Re = 4.9, a single particle released off-center migrates toward the centerline.
- Hydrodynamic forces between the particle and the walls are in balance.





Simulations of two particles				
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Consider two initial configurations, centered and off-center, with particles separated by a distance 2D:



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Two particles at low Re: Drafting and kissing

At low Reynolds number (Re = 3), the particles approach each other (draft) and nearly touch (kiss):



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Two particles at Re = 80: DKT behaviour

At higher Reynolds number (Re = 80), the particles undergo a tumbling motion after drafting and kissing:



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Two particles at Re = 80: DKT behaviour (cont'd)



Results match qualitatively with FEM simulations of Feng, Hu & Joseph (1994).

[Video]

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Two particles at Re = 47, off-center

More interesting behaviour arises at an intermediate Reynolds number (Re = 47) for two particles released off-center:



[Video]

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Closing remarks

- We developed a 2D immersed boundary method that handles gravitational settling in the presence of walls.
- Computed settling velocities match with experiments.
- More complicated two-particle dynamics are consistent with simulations of Feng, Hu & Joseph (1994).

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Current and future work

- Study settling of deformable, non-spherical particles.
- Investigate applications to:
 - biofilm floc deformation,
 - flexible fiber suspensions,
 - jellyfish swimming dynamics.
- Simulate large numbers of particles using Wiens' parallel IB algorithm. [Wiens & JS, submitted to *J. Comput. Phys.*, arXiv:1305.3976, 2013]



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Thank-you!

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