symmetrically along the barrier. Calculate the horizontal force F needed, per unit thickness into the paper, to hold the barrier stationary.

Solution: For water take $\rho = 998$ kg/m. The control volume (see figure) cuts through all four jets, which are numbered. The velocity of all jets follows from the weight flow at (1):

$$V_{1,2,3,4} = V_1 = \frac{\dot{w}_1}{\rho g A_1} = \frac{1960 \, N/s}{(9.81m/s^2)(998kg/m^3)(0.04m)(1m)} = 5.0 \frac{m}{s}$$

$$\dot{m}_1 = \frac{\dot{w}_1}{g} = \frac{1960N/s - m}{9.81N/s^2} = 200 \frac{kg}{s - m}; \\ \dot{m}_2 = 0.3\dot{m}_1 = 60 \frac{kg}{s - m}; \\ \dot{m}_3 = \dot{m}_4 = 70 \frac{kg}{s - m}$$

Then the *x*-momentum relation for this control volume yields

$$\Sigma F_x = -F = \dot{m}_2 u_2 + \dot{m}_3 u_3 + \dot{m}_4 u_4 - \dot{m}_1 u_1 = -F = (60)(5.0) + (70)(-5.0\cos 55^\circ) + (70)(-5.0\cos 55^\circ) - 200(5.0), \text{ or }:$$

$$F = 1000 + 201 + 201 - 300 \approx 1100 \text{ N per meter of width } Ans.$$

3.31 A bellows may be modeled as a deforming wedge-shaped volume as in Fig. P3.31. The check valve on the left (pleated) end is closed during the stroke. If *b* is the bellows width into the paper, derive an expression for outlet mass flow \dot{m}_o as a function of stroke $\theta(t)$.



Solution: For a control volume enclosing the bellows and the outlet flow, we obtain

Fig. P3.31

$$\frac{d}{dt}(\rho v) + \dot{m}_{out} = 0$$
, where $v = bhL = bL^2 \tan \theta$

since L is constant, solve for
$$\dot{m}_0 = -\frac{d}{dt}(\rho bL^2 \tan \theta) = -\rho bL^2 \sec^2 \theta \frac{d\theta}{dt}$$
 Ans.