4.41 As mentioned in Sec. 4.10, the velocity profile for laminar flow between y = h

 $u = \frac{4u_{\max}y(h-y)}{h^2} \qquad v = w = 0$ 

two plates, as in Fig. P4.40, is



the incompressible-flow energy equation (4.75) to solve for the temperature distribution T(y) between the walls for steady flow.

**Solution:** Assume T = T(y) and use the energy equation with the known u(y):

$$\rho c_{p} \frac{DT}{dt} = k \frac{d^{2}T}{dy^{2}} + \mu \left(\frac{du}{dy}\right)^{2}, \text{ or: } \rho c_{p}(0) = k \frac{d^{2}T}{dy^{2}} + \mu \left[\frac{4u_{max}}{h^{2}}(h-2y)\right]^{2}, \text{ or:}$$
$$\frac{d^{2}T}{dy^{2}} = -\frac{16\mu u_{max}^{2}}{kh^{4}}(h^{2} - 4hy + 4y^{2}), \text{ Integrate: } \frac{dT}{dy} = \frac{-16\mu u_{max}^{2}}{kh^{4}}\left(h^{2}y - 2hy^{2} + \frac{4y^{3}}{3} + C_{1}\right)$$

Before integrating again, note that dT/dy = 0 at y = h/2 (the symmetry condition), so  $C_1 = -h^3/6$ . Now integrate once more:

$$\Gamma = -\frac{16\mu u_{\text{max}}^2}{kh^4} \left( h^2 \frac{y^2}{2} - 2h \frac{y^3}{3} + \frac{y^4}{3} + C_1 y \right) + C_2$$

If  $T = T_W$  at y = 0 and at y = h, then  $C_2 = T_W$ . The final solution is:

$$T = T_{w} + \frac{8\mu u_{max}^{2}}{k} \left[ \frac{y}{3h} - \frac{y^{2}}{h^{2}} + \frac{4y^{3}}{3h^{3}} - \frac{2y^{4}}{3h^{4}} \right] Ans.$$

**4.42** Suppose that we wish to analyze the rotating, partly-full cylinder of Fig. 2.23 as a *spin-up* problem, starting from rest and continuing until solid-body-rotation is achieved. What are the appropriate boundary and initial conditions for this problem?

**Solution:** Let V = V(r, z, t). The initial condition is: V(r, z, 0) = 0. The boundary conditions are

Along the side walls:  $v_{\theta}(R, z, t) = R\Omega$ ,  $v_{r}(R, z, t) = 0$ ,  $v_{z}(R, z, t) = 0$ . At the bottom, z = 0:  $v_{\theta}(r, 0, t) = r\Omega$ ,  $v_{r}(r, 0, t) = 0$ ,  $v_{z}(r, 0, t) = 0$ .