

Thermal performance of aerogel blanket insulation

by

Atiyeh Hoseini

M.Sc., Sharif University of Technology, 2013

B.Sc., Sharif University of Technology, 2011

Thesis Submitted in Partial Fulfillment of the
Requirements for the Degree of
Doctor of Philosophy

in the

School of Mechatronic Systems Engineering
Faculty of Applied Sciences

© Atiyeh Hoseini

SIMON FRASER UNIVERSITY

Fall 2017

Copyright in this work rests with the author. Please ensure that any reproduction or re-use is done in accordance with the relevant national copyright legislation.

Approval

Name: Atiyeh Hoseini

Degree: Doctor of Philosophy

Title: Thermal performance of aerogel blanket insulation

Examining Committee:

Chair: Kevin Oldknow
Senior Lecturer

Majid Bahrami
Senior Supervisor
Professor

Byron Gates
Supervisor
Associate Professor
Department of Chemistry

Woo Soo Kim
Supervisor
Associate Professor

Gary Leach
Internal Examiner
Associate Professor
Department of Chemistry

Ralph Evins
External Examiner
Assistant Professor
Department of Civil Engineering
University of Victoria

Date Defended/Approved: September, 08, 2017

Abstract

Population growth has significantly increased the energy consumption of the building sector, which is currently 32% of the total global energy demand. Energy use for residential and commercial heating and cooling is projected to strongly grow until 2050, increasing by 79% and 84%, respectively, compared to 2010 [1]. Development of high performance thermal insulation materials is crucial to saving space and energy, increasing comfort, and decreasing environmental impact, cost, and complexity. Aerogels are a promising high-performance type of thermal insulation for both stationary and mobile applications. The thermal performance of insulations is typically judged by their reported R-value (thermal resistance); however, this value may differ from the in-service R-value for reasons such as temperature and humidity variations as well as mechanical compression.

In this research, the thermal performance of aerogel blanket super insulation is thoroughly studied under various operating conditions, i.e., temperature, compression, and humidity. The microstructure of commercially available aerogel blankets was characterized using microscopy, porosimetry and spectroscopy. A comprehensive set of accurate analytical models were developed and verified experimentally to predict the thermal and mechanical performance of aerogel blankets in dry and humid conditions. These models can be utilized to predict the thermal performance of the insulation for building envelopes and other large-scale applications. Furthermore, the design of such materials can be improved by performing an optimization study on the microstructural and morphological properties of aerogel blankets using the developed analytical models.

The results of the aerogel blanket performance modeling and measurements indicated that mechanical load on the material, elevated temperature and high humidity decrease the R-value of aerogel blankets. These factors should be considered in the thermal insulation design and selection for an application to benefit the most from this super insulation material.

Keywords: Aerogel blankets; Super insulation materials; Heat transfer; Mechanical performance; Thermal performance; Characterization

*To my beloved mother, my lovely sister Leyla and the love of my
life Amir Abbas*

Acknowledgements

I would like to thank my senior supervisor, Dr. Majid Bahrami, for his support and guidance throughout my Ph.D. studies. It has been a privilege to work with him and learn from his experience.

I am also thankful to my supervisory committee members, Dr. Woo Soo Kim and Dr. Byron Gates, for their discussions and comments on my research project. I am also thankful to Dr. Evins and Dr. Leach for their time reading this thesis and comments. Also, I am grateful to Dr. Oldknow for being the defense committee chairman.

I would like to thank my friends and colleagues at Laboratory for Alternative Energy Conversion (LAEC) at Simon Fraser University for their support and contributions. Specially, I thank Dr. Claire McCague, LAEC's previous manager, Marius Haiducu, and LAEC's engineers, Dr. Wendell Huttema and Dr. Mehran Ahmadi, who supported this research project.

I would also like to thank the Natural Sciences and Engineering Research Council of Canada (NSERC) for the financial support through the Automotive Partnership Canada Grant.

Last but not the least; I would like to express my gratitude to my mother and my sister for their endless support and encouragement in all stages of my life. My special thanks go to my husband, Amir Abbas, for his support, and encouragement throughout my professional career. None of these would have been possible without the love and patience of my family.

Table of Contents

Approval.....	ii
Abstract.....	iii
Dedication.....	iv
Acknowledgements.....	v
Table of Contents.....	vi
List of Tables	viii
List of Figures	ix
List of Acronyms	xi
Nomenclature	xii
Executive Summary	xiv
Objectives.....	xv
Methodology.....	xv
Contributions	xvi
References.....	xvii
Chapter 1. Introduction.....	1
1.1. Research Importance and Background	1
1.2. Relevant Literature	5
1.2.1. Temperature Effect.....	6
1.2.2. Humidity Effect	10
1.2.3. Mechanical Compression Effect	12
1.2.4. Lack of the Literature.....	15
Chapter 2. Thermal Analysis of Aerogel Blankets	16
2.1. Mechanisms of Heat Transfer in Insulations	17
2.1.1. Conduction	17
2.1.2. Convection	17
2.1.3. Radiation.....	17
2.1.4. Effective Thermal Conductivity	18
2.2. The present Model	18
2.2.1. Conduction heat transfer	20
Thermal conductivity of the porous medium around the fiber containing dry air and aerogel particles	21
Thermal conductivity of the porous medium around the fiber at humid conditions.....	23
Moisture supplement for the thermal conductivity (Z constant).....	28
2.2.2. Radiation heat transfer	29
2.3. Experimental study.....	31
2.3.1. Thermal Conductivity Measurements of the Dry Samples	33
2.3.2. Moisture Content Measurements.....	34
2.3.3. Thermal conductivity Measurements of the Samples at Different Levels of RH	35
2.4. Results and Discussion	36
2.4.1. Model Validation and Parametric Studies for the Dry Samples	37

2.4.2. Model Validation and Parametric Studies for the Samples at Different Levels of RH ..	43
.....	43
Sorption isotherm measurements	43
Thermal conductivity analysis at the transient regime	44
Thermal conductivity analysis at the steady-state regime	48
Chapter 3. Mechanical Deformation Analysis of Aerogel Blankets	51
3.1. The Present Model	51
3.2. Experimental Study	57
3.3. Results and Discussion	58
Chapter 4. Combined Thermal and Mechanical Deformation Analysis of Aerogel Blankets	64
4.1. The Present Model	64
4.2. Experimental Study	65
4.3. Results and Discussion	65
Chapter 5. Summary and Future Work	70
References	74
Appendix A. Pore size measurement	85
Appendix B. Experimental data	87
Cryogel [®] Z.....	88
ThermalWrap	91
Appendix C. Uncertainty Analysis	94
Appendix D. Total Heat Transfer Governing Equations	95

List of Tables

Table 1-1.	Summary of literature on the effect of temperature on aerogel blanket thermal performance.....	8
Table 1-2.	Summary of the available studies on aerogel and aerogel-based composites at humid conditions.	12
Table 1-3.	Summary of available studies on thickness or density of aerogel-based composites.....	14
Table 2-1.	Table of equivalent parameters in electrical and mass transfer systems.	25
Table 2-2.	Aerogel blanket samples specifications.....	31
Table 2-3.	Diffusion parameters of CZ at different RH.....	47
Table 3-1.	Constant parameters used in the compression analytical model.	59

List of Figures

Figure 1.	Scope and deliverables of the present research project.....	xviii
Figure 2.	(a) Fine particles of aerogel, (b) aerogel blanket	5
Figure 3.	Proposed unit cell for aerogel blanket geometrical modeling.....	19
Figure 4.	Schematic of the moisture distribution inside the pores of the proposed unit cell; small blue circles depict adsorbed water.....	24
Figure 5.	Zero-dimensional (lumped) RC model of aerogel blanket insulation material in humid conditions.	25
Figure 6.	FTIR spectra of (a) CZ, and (b) TW aerogel blankets. ν shows stretching bond vibration, δ bond bending vibration and a asymmetric bond vibration.....	33
Figure 7.	(a) The HFM instrument, and (b) its schematic.	34
Figure 8.	Device (a) and simplified schematic of TPS (Transient Plane Source) thermal conductivity measurement (b).	36
Figure 9.	Temperature dependence of the thermal conductivity of dry CZ and TW aerogel blankets.	38
Figure 10.	Contribution of each type of heat transfer (%) on total heat transfer rate; (a) CZ, and (b) TW.....	39
Figure 11.	Effect of fiber material thermal conductivity on the effective thermal conductivity	40
Figure 12.	Effect of blanket porosity on the effective thermal conductivity.....	41
Figure 13.	Effect of deformed factor on the effective thermal conductivity.....	41
Figure 14.	Thermal conductivity variation during temperature cycling for CZ, (a) 10 mm, and (b) 5 mm thickness.....	42
Figure 15.	Thermal conductivity variation during temperature cycling for TW, (a) 8 mm, and (b) 5 mm thickness.....	43
Figure 16.	Sorption isotherms at 25°C and 45°C for CZ and TW aerogel blanket samples.	44
Figure 17.	CZ weight increase in three cases: blue line: actual measured data; red line: water vapor filled the pores; and green line: adsorbed water.	44
Figure 18.	Cyclic thermal conductivity measurements of CZ and TW between 0% and 80% RH at 25°C.....	45
Figure 19.	Thermal conductivity of CZ over time at 25°C and 20%, 40% and 80% RH.	46
Figure 20.	Sensitivity analysis on CZ diffusion coefficient at 20% RH and 25°C.	47
Figure 21.	Moisture volume fraction of CZ over time at 25°C.	48
Figure 22.	Effective thermal conductivity as a function of RH for CZ at 25°C and 45°C.	49
Figure 23.	Effective thermal conductivity as a function of RH for TW at 25°C and 45°C.....	49
Figure 24.	The change in the thermal conductivity as a function of moisture content at 25°C	50
Figure 25.	(a) SEM image of aerogel blanket (CZ) showing aerogel coated fibers (marked with dotted lines) and aerogel filled pores, and (b) Geometry of the proposed unit cell, and (c) schematic of the solution domain showing fibers coated with a layer	

	of aerogel particles, a larger spherical aerogel particle at the center, a force, F' , applied to the uppermost fiber and the fibers length in the unit cell, l_{fiber}	52
Figure 26.	(a) Schematic of the applied beam theory, and (b) the solution domain used in stress-strain analysis.	54
Figure 27.	Porosity modification algorithm.	56
Figure 28.	(a) TMA device, and (b) its schematic [104]	57
Figure 29.	Microstructure of aerogel blanket samples; at no-load and compressed conditions. The scale bars show 100 μm	58
Figure 30.	Stress-strain data and modeling result for CZ with 5 mm nominal thickness.	60
Figure 31.	Stress-strain data and modeling result for TW with 5 mm nominal thickness.	60
Figure 32.	Stress-strain data and modeling result for CZ with 10 mm nominal thickness.	60
Figure 33.	Stress-strain data and modeling result for TW with 5 mm nominal thickness.	60
Figure 34.	Effect of aerogel particle size on aerogel blanket strain.....	61
Figure 35.	Effect of fiber diameter on aerogel blanket strain	61
Figure 36.	Cycle test for load range of 0.7-2 kPa for thinner samples and 0.7-5 kPa for thicker ones	63
Figure 37.	Thermal resistance modeling methodology	65
Figure 38.	Total resistance variation as a function of thickness at $T=25^{\circ}\text{C}$ and $\text{RH}=0\%$	66
Figure 39.	Resistance variation of CZ of 5 mm nominal thickness and TW of 5 mm nominal thickness at various compressive loads at $T=25^{\circ}\text{C}$ and $\text{RH}=0\%$	67
Figure 40.	Resistance variation of CZ of 10 mm nominal thickness and TW of 8 mm nominal thickness at various compressive loads at $T=25^{\circ}\text{C}$ and $\text{RH}=0\%$	67
Figure 41.	Resistance variation of CZ of 5 mm nominal thickness at various compressive loads at $T=25^{\circ}\text{C}$ and changing RH.....	68
Figure 42.	Resistance variation of CZ of 5 mm nominal thickness at various compressive loads at $\text{RH}=0\%$ and changing temperature. The data are experimental results from HFM.....	68

List of Acronyms

ASHRAE	American Society of Heating, Refrigeration, and Air Conditioning Engineers
ASTM	American Society for Testing Materials
EIA	Energy Information Administration
FTIR	Fourier Transform Infrared Spectroscopy
GHG	Greenhouse gas
HFM	Heat Flow Meter
ISO	International Organization for Standardization
MIP	Mercury Intrusion Porosimetry
RH	Relative Humidity
SEM	Scanning Electron Microscopy
TPS	Transient Plane Source
TMA	Thermo-Mechanical Analyzer

Nomenclature

A	Area (m^2)
D	Diffusion coefficient ($\text{m}^2\cdot\text{s}^{-1}$)
e_b	Blackbody emissive power
e	Strain
m	Mass
x	Volume fraction
EI	Effective flexural rigidity ($\text{N}\cdot\text{m}^2$)
EJ	Exajoules
F	Force (N)
k	Thermal conductivity ($\text{W}\cdot\text{m}^{-1}\cdot\text{K}^{-1}$)
K_R	Mean extinction coefficient
Kn	Knudsen number
l	Length (m)
t	Thickness (m)
n	Index of refraction
N	Number
ϕ	Heat flux ($\text{W}\cdot\text{m}^{-2}$)
R	Resistance
r	Radius (m)
T	Temperature (K)
$T_{n\lambda}$	Spectral transmittance
c	Concentration ($\text{kg}\cdot\text{m}^{-3}$)
V	Volume (m^3)
P	Pressure (Pa)

Greek Symbols

α	Deformed factor
β	Extinction coefficient
ε	Porosity
δ	Deformation (m)
λ	Wavelength (m)
σ	Stefan-Boltzmann constant
γ	Stress (Mpa)

ω	Water content
ϕ	Volume fraction
Λ	Mean free path
Subscripts	
app	Apparent
b	Blanket
cond.	Conduction
eff	Effective
f	Fiber
g	Gas
gs	Gas solid region
m	Medium
s	Solid
tot	Total
u	Unit cell
rad.	Radiation
w	Water
v	Vapor

Executive Summary

The building sector is the largest energy-consuming sector, accounting for over one-third of final global energy consumption, as well as being a significant source of carbon dioxide emissions [2]. As people spend more times in the buildings, there will be an upward trend in energy demand of both residential and commercial buildings in the future [3]. By 2050, an estimated 40 exajoules (EJ) of energy, equivalent to the current energy use in Russia and India combined, could be saved in the building sector through the wide deployment of the best available technologies in the building envelope and its insulation, space heating and cooling systems, water heating, lighting, etc.[2]. Development of high-performance thermal insulation materials is a key to save space and energy, increase comfort, and decrease environmental impacts and costs. Among available insulating materials, aerogels are promising high performance materials for both stationary and mobile applications. Aerogel-based composites have the lowest thermal conductivity of any known insulation materials, providing the highest insulation properties for maximum energy efficiency accompanying less weight and thickness, and high flexibility and hydrophobicity. Aerogel-based composites also have zero Ozone Depleting Potential (ODP), which is the relative amount of degradation a chemical compound can cause to the ozone layer [4].

Aerogel, although discovered in 1960, is still not a common material and the current fundamental understanding of this material is primarily empirical. Urgent actions are needed to ensure that high-performance building envelopes rapidly gain market share and quickly become the standard for all new constructions globally. As such, aerogel blanket technology has begun receiving particular attention recently in the universal insulation market due to its prominent thermal performance [4]. This technology can address challenges posed by high-energy demands of residential and commercial buildings, where waste energy and greenhouse gas (GHG) emissions are major concerns. This research focuses on the material characterization and performance evaluation of the ultralight aerogel blanket super thermal insulation materials that provide much higher insulation property (R-values) and slower degradation over time.

Objectives

The research objectives are as follows:

- Develop an in-depth understanding of various heat transfer mechanisms involved in super thermal insulation materials and their relationship with salient micro structural parameters, such as porosity, fiber shape, size, and material.
- Characterize and study the performance of aerogel blanket super thermal insulation material in buildings. The main focus is placed on building envelopes, however; the developed models can be used in the transportation industry as well as urban farms and greenhouses to significantly reduce their energy loss, and their environmental impacts.
- Provide a platform for predicting the thermal and mechanical performance of an enclosure, insulated using aerogel blankets under realistic conditions of temperature, humidity, and mechanical compression.

Methodology

The thesis structure and research roadmap for accomplishing the objectives is shown in Figure 1. The project is broken into two main parts; i) modeling and ii) experiments. Each part is treated separately, with different methodologies, to fill the gap in the existing literature. At the end, the results from different parts are combined and used to develop an accurate model to evaluate the thermal performance of aerogel blankets under realistic conditions.

Specifically, this research is focused on investigating: i) the effects of microstructural and morphological properties on the effective insulation value (thermal conductivity); and ii) the effects of operating conditions, i.e., temperature, relative humidity (RH), and mechanical compression on thermal properties of such porous structures. Our research utilizes advanced imaging equipment, e.g., scanning electron microscopy (SEM), as well as mercury intrusion porosimetry (MIP), and Fourier transform infrared spectroscopy (FTIR) as a starting point for characterization of the micro-/nano-structure that is the key for analytical modeling of aerogel blankets.

In this study, analytical thermal and mechanical models are developed for aerogel blankets using a unit-cell approach that is capable of relating the material properties to its micro-

structure. The mathematical model accurately predicts the thermal conductivity (or R-value) of highly porous insulation materials such as aerogel blankets under operating conditions (temperature, RH, and compression). The accuracy of the analytical model is verified using the acquired data from the experimental studies.

On the experimental front, thermal, mechanical and optical measurements are conducted using commercially available samples of aerogel blankets. Two types of apparatus for measuring thermal conductivity of porous insulation sheets are used: i) Heat Flow Meter (HFM) as per ASTM C518, ISO 8301, JIS A1412, and DIN EN 12667 standards; and ii) Transient Plane Source (TPS) as per ISO Standard 22007-2. Also, a thermomechanical analyzer (TMA) is used to measure the deformation of aerogel blankets under different mechanical loads. Additionally, to investigate the effect of moisture diffusion on thermal performance of aerogel blankets, TPS capability is improved by coupling it with a humidifier. This has been a major milestone in this research.

Contributions

The following provides an overview of the main contributions of this study:

- Developed a new geometrical model, using the concept of “unit cell”, to represent the salient microstructural characteristics of aerogel blankets [1, 2].
- Developed and verified a new analytical thermal model to predict the effect of temperature on thermal performance (R-value) of aerogel blankets [1, 2].
- Developed an analytical mass transfer model to predict the water content of aerogel blankets at various temperature and humidity conditions over time [3, 4].
- Extended the analytical thermal model to humid conditions to predict the effect of moisture diffusion and temperature on thermal performance of aerogel blankets [3, 4].
- Developed and validated a new analytical mechanical model to predict the deformation of aerogel blankets under uniaxial compression [5, 6].
- Performed several experimental studies to examine the thermal performance of aerogel blankets exposed to continuous cyclic conditions of temperature, humidity, and mechanical compression [1-6].

- Combined the above-mentioned sub-models into a unified and robust analytical model that is capable of accurately predicting thermal conductivity (R-value) accounting for all salient geometrical parameters, as well as operating conditions (temperature, RH, and compression) for aerogel blankets [5, 6].

References

- [1] A. Hoseini, C. McCague, M. Andisheh-Tadbir, and M. Bahrami, "Aerogel blankets: From mathematical modeling to material characterization and experimental analysis," *Int. J. Heat Mass Transf.*, vol. 93, pp. 1124–1131, 2016.
- [2] A. Hoseini, M. Andisheh-Tadbir, and M. Bahrami, "Aerogel blanket insulation: Experimental validation of analytical thermal conductivity model," 13th SOL-GEL conference, Kyoto, Japan, September 2015 (Poster).
- [3] A. Hoseini and M. Bahrami, "Effects of humidity on thermal performance of aerogel insulation blankets," *J. Build. Eng.*, vol. 13, no. July, pp. 107–115, 2017.
- [4] A. Hoseini, M. Bahrami, "Effect of moisture builds up on thermal conductivity of aerogel blankets," 12th Conference on Advanced Building Skins, Bern, Switzerland, October 2017 (Oral presentation).
- [5] A. Hoseini, A. Malekian, and M. Bahrami, "Experimental investigation and analytical modeling of aerogel blanket deformation and thermal performance variation under compression," 27th International Symposium on Transport Phenomena, Honolulu, September 2016 (Oral presentation).
- [6] A. Hoseini, A. Malekian, and M. Bahrami, "Deformation and thermal resistance study of aerogel blanket insulation material under uniaxial compression," *Energy and Buildings*, vol. 130, pp. 228–237, 2016.

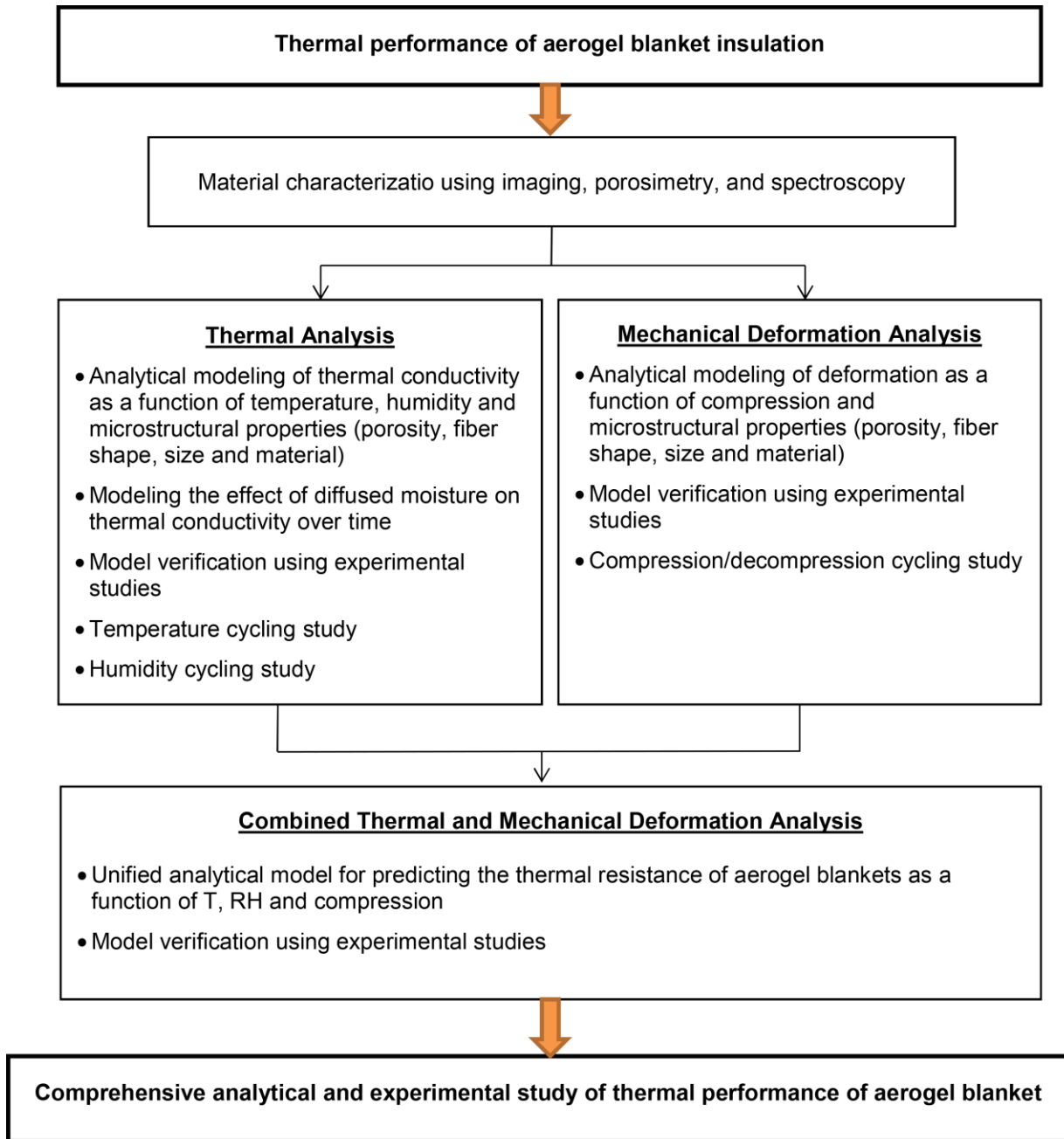


Figure 1. Scope and deliverables of the present research project.

Chapter 1.

Introduction

1.1. Research Importance and Background

As energy becomes more costly and demand grows, the use of efficient thermal insulations in buildings becomes more serious. Energy consumption in buildings accounts for 20-40% of the total energy consumption in developed countries. The growth of building energy consumption in Europe and North America is 1.5% and 1.9% per year, respectively [3]. As the U.S. Energy Information Administration (EIA) predicted in the International Energy Outlook [5], in 2030, energy consumption of houses and the non-domestic sectors will be ~67% and ~33%, respectively. By adding insulation, the amount of energy needed to heat the buildings will be lowered, which results in fewer associated greenhouse gas (GHG) emissions and lower monthly heating expenses. The thermal performance of the building envelope depends critically on the thermal effectiveness of the insulation layer. Cabeza et al. [6] performed an experimental study on the energy performance of three typical insulation materials; polyurethane, polystyrene, and mineral wool. Four house-like cubicles were built and their thermal performance over the time was measured under the normal climatic conditions. Energy reductions up to 64% in summer and up to 37% in winter were reported. Thermal performance of building insulation is mainly determined by its k-value (thermal conductivity value) or R-value (thermal resistance value). The k-value depends on the material density, porosity, moisture content, and average temperature difference. Reported k-values by manufacturers are normally assessed at standard laboratory conditions of temperature, humidity, and mechanical load to allow a comparative evaluation of the thermal performance. However, when placed in their locations in the building envelope, thermal insulation materials are exposed to different circumstances depending on the prevailing climatic conditions, hence their actual thermal performance may be extensively different from that anticipated performance under standard laboratory conditions. This may result in major deviations in predicting the thermal and energy performance of the whole building. Abdou et al. [7] examined the variation of the k-value of seven insulation materials (*i.e.*, fiberglass, wood wool, mineral wool, rock wool, polyethylene, polyurethane, and polystyrene) under different operating temperatures. Their results showed that higher temperature leads to higher k-values and that higher insulation density generally results in lower thermal conductivity. Bo-Ming et al. [8] measured the effective

thermal conductivities of a fibrous insulation at the temperature range of 300 to 973 K and claimed that effective thermal conductivity increases non-linearly with increasing average temperature of the sample. They also developed a one dimensional finite volume numerical model combining radiation and conduction heat transfer to predict the behavior of the effective thermal conductivity of the fibrous insulation at various temperatures and pressures. However, in the mentioned studies the impact of accumulation of moisture within the investigated insulations and the subsequent reduction of the insulation thermal resistance, which is another major factor affecting the k-value of insulation materials, was not considered. The ambient air humidity and indoor conditions, as well as the wall or roof system moisture characteristics, play an important role in determining the moisture status of the insulation material. In hot–humid climates, condensation can happen within the insulation material, raising its moisture content. This leads to higher thermal conductivity due to the enhanced heat transfer by conduction and, under certain conditions, by the evaporation–condensation process, in which moisture moves from warm to cold regions. The presence of moisture in insulation may also contribute to corrosion and degradation under the insulation layer. Additionally, moisture buildup can result in the growth of fungus and mold, which can affect the structural reliability of building components and occupants' health [9-11]. Fan and Wen [12] and Fan et al. [13] studied the initial water content and thickness of the fibrous insulation together with the environmental temperature as the three most important factors influencing the heat flux. Björk and Enochsson [14] studied the moisture dependent heat transfer for three different thermal insulation materials: glass wool, melamine foam, and corrugated sheets of cellulose plastic. The materials were quite different with respect to condensation formation and maximal moisture accumulation at similar environmental conditions. They also showed considerable differences in moisture influence on the heat transfer. Their results showed that the higher the moisture accumulation, the greater the influence of the moisture on thermal transmissivity at a steady-state condition.

Thermal insulations can be categorized in different ways [15] , based on their:

- a) Structure : porous(foam), fibrous, and granulated;
- b) Shape of product: loose (back fill, wool) and flat (board, mat, felt);
- c) Binder content: containing binder and binder-free;
- d) Type of ground substance: inorganic and organic; and

- e) Reaction to fire (Euroclass): non-combustible (class A1), limited combustibility (class A2, B), combustible (class C, D, E, F).

Insulation products can also be classified according to the nature of their material [16]:

- a) Light silicate substances, *e.g.*, light aggregate, light concrete;
- b) Foam inorganic substances, *e.g.*, foam glass;
- c) Foam organic substances, *e.g.*, foam plastics;
- d) Fibrous substances, *e.g.*, glass wool and mineral (stone) wool; and
- e) Organic substances, *e.g.*, cork, timber wool, and paper.

Each type of insulation material has advantages and disadvantages, in terms of durability, material stability, resistance to fire, and impact on environment and human health. Therefore, the type of the building and local conditions specify the choice of the right insulation. Aerogel-based composite materials are also a member of building insulation materials that can protect buildings and constructions against changes of the ambient conditions and are recently being investigated due to their enhanced thermal properties. By using aerogel-based composite materials, thinner walls can be built having the same insulation R-value compared to conventional insulation materials. This characteristic is useful in big cities where space allocation is limited for new constructions and also represents an economic benefit for the owner.

Aerogels were invented in 1930 by Dr. Samuel Stephens Kistler; however, their first commercialization did not happen until the 1950s [17]. The three most common types of aerogels are silica, carbon and metal oxides, but it is silica that is most often used experimentally and in practical applications. Silica is a glassy material often used for insulation. Unlike the smoky-blue silica aerogels, carbon-based aerogels are black and feel like charcoal. They have high surface area and are electrically conductive. These properties make carbon aerogels useful for supercapacitors, fuel cells and desalination systems. Metal oxide aerogels are used as catalysts for chemical transformations. They are also used in the production of explosives and carbon nanotubes, and these aerogels can even be magnetic. Aerogels are manufactured through a supercritical drying process that creates a highly porous open cell solid material, which feature thermal conductivities as low as $0.013 \text{ W}\cdot\text{m}^{-1}\cdot\text{K}^{-1}$ [18]. More details of the methodology used in the aerogel synthesis can be found in Ref. [19]. Their remarkable properties include extremely

low thermal conductivity, high resistance to acoustic waves, and low dielectric constant. Aerogels function as thermal super insulators mainly by minimizing heat conduction through their low density and tortuous solid nanostructure; heat convection through very small pore sizes; and radiation by adding infrared (IR) absorbing or scattering agents in the aerogel matrix. Super-insulating silica-based aerogels are low density, typically in the range of 0.08 to 0.2 g·cm⁻³, nanostructured solids with a high porosity (>95%) and typical mesopore diameters. However, aerogels have a delicate structure with low compressive strength and high susceptibility to fracture, which make them difficult to handle. They are also prone to settling over time, especially when exposed to vibration or thermal cycling. The settling process can form voids and lead to heat leakage in the void spaces, which is a major drawback for any powder-based insulation [20]. Therefore, more durable aerogel composites, known as fiber-reinforced aerogel blankets, have been developed. These materials have applications in aerospace, military cryogenic applications, the oil and gas processing industry, and construction [4]. Aerogel blankets contain aerogel particles, fibers, and optionally, a binder. In other words, in order to be of practical use as a thermal insulator, aerogels are combined with other materials to improve strength, while retaining the aerogel's desirable properties. Aerogel composites typically involve molding a gel around a supporting structure (e.g., lofty fibrous batting, xonotlite-type calcium silicate [21]), followed by the drying process. The aerogel and supporting structure can also be combined after formation of the aerogels. The material is mechanically stable and has low thermal conductivity ranging between 0.017 to 0.04 W·m⁻¹·K⁻¹ [22]. Figure 2 shows fine particles and a sample of an aerogel blanket. In this work, we will investigate the available literature on aerogel blankets. The goal is to study their thermal performance under various environmental conditions; e.g., temperature, humidity, and mechanical compression, by proposing a unified mathematical modeling for these factors. Subsequent experimental analysis will be done using different equipment, such as, HFM, TPS, humidifier, TMA, SEM, and MIP. The proposed models will be introduced as a package for predicting the thermal performance of a building insulated using aerogel blankets.

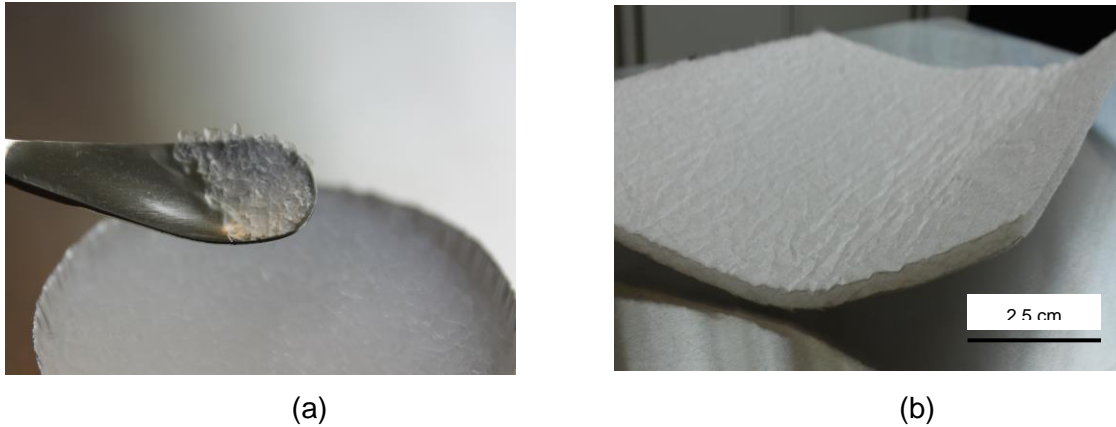


Figure 2. (a) Fine particles of aerogel, (b) aerogel blanket

1.2. Relevant Literature

The parameters that contribute to the variation of the thermal insulation R-value or its thermal conductivity are documented in the ASHRAE Handbook of Fundamentals [23]. These factors emphasize three major issues: temperature variation, mechanical abuse, and moisture penetration, which can lead to a drastic change in the expected R-value. The effect of these parameters has been long considered in building envelopes, for conventional insulation materials, as a source of a reduced quality of living and a reason of permanent damage to the building structures. Although some of these factors can be reduced by better planning and thorough monitoring, some others cannot be completely avoided and lead to slow degradation and significant decrease in insulating properties of a building material. Therefore, more research is needed to be done in anticipating the thermal performance of an insulation material under various environmental conditions and also over time.

Aerogels are being investigated recently for building and transportation applications. The most common method for improving the strength of silica aerogel is adding reinforcing fibers into aerogel (it is called aerogel blanket), which also results in less conduction and radiation heat transfer. The proper fiber selection can strongly reduce the radiative heat transfer by increasing scattering and absorption [24], [25]. Manufacturers, Aspen Aerogel Inc. and Cabot Aerogel Corporation, have reported the properties of their aerogel-based products as a function of density, pressure, and composition [22]. Kyung Wha Oh et al. [26] produced a flexible and mechanically strengthened hybrid, polyethylene terephthalate (PET)/aerogel blanket, by embedding the aerogel in a nonwoven fiber matrix as a sound and thermal insulation material. The PET/aerogel blanket was produced by two methods; one is direct gelation of silica on nonwoven PET and the

other is dipping of PET in the dispersion of silica hydrogel. Their developed hybrid PET/aerogel showed better acoustical and thermal performances compared to monolithic aerogels. Overall, aerogel blankets thermal conductivity can be lower than air at the same pressure and their exceptional insulation characteristics are due to the small size of the large number of pores. Aerogel blankets are thin (less than 10 mm), which makes them an ideal choice for space-constrained locations. Additionally, aerogel blankets may be used from cryogenic to high temperatures ($<-196^{\circ}\text{C}$ to $>800^{\circ}\text{C}$). Summary of the major findings of the literature review is classified in the following sections.

1.2.1. Temperature Effect

Several experimental studies have been done for evaluating heat transfer mechanisms in dry aerogel blanket insulations. A heat transfer model based on the structure of aerogel-based composites is needed to understand their characteristics at various conditions. The first effective thermal conductivity model was developed based on superposition of the solid and gas conduction and radiation thermal conductivities [27]. Convective heat transfer is negligible when the pore sizes are smaller than 1 mm [25, 28]. The second type of models uses radiation and a combined solid and gas conduction [28, 29]. The combined solid and gas thermal conductivity was developed based on a periodic structure simplified from the real material structure or an empirical combined parallel and series thermal resistance model. Wei et al. [30] investigated the effective thermal conductivity of xonotlite-aerogel composite, which was a combination of hollow spherical agglomerates interwoven with xonotlite-type calcium silicate fibers. They developed theoretical and experimental analysis on thermal conductivity of silica aerogel, xonotlite-type calcium silicate, and xonotlite-aerogel composite insulation material. They modeled one dimensional heat transfer by assuming a periodic array of hollow cubic structures with connecting bars. In this model, gas and solid conduction and radiative heat transfer were considered as the modes of heat transfer inside the composite. The model accurately predicted the thermal conductivity of a specific aerogel blanket in various pressures, temperatures, and density ranges. Their results showed that effective thermal conductivity can be lowered significantly by the composite of aerogel and xonotlite-type calcium silicate at higher temperatures. The third type of modeling was developed using numerical calculations based on the meshing of the actual structure. Although the third type is more time-consuming and cannot give analytical results, it gives more precise predictions than the other two methods. Coquard et al. [31] developed a numerical model for estimating the conductive heat transfer inside nano-structured silica using a

representation of their porous structure. The model took into account the porous morphology of the material at both nano and microscopic scales. A summary of the literature on the effect of temperature on dry aerogel blanket thermal performance studies is presented in Table 1-1.

Table 1-1. Summary of literature on the effect of temperature on aerogel blanket thermal performance.

Author(s)	Notes
Kyung Wha Oh et al. [26]	<ul style="list-style-type: none"> • Synthesized flexible, mechanically strengthened hybrid of PET/aerogel blanket using two different methods of drying under ambient pressure • Performed experimental study on the acoustic and thermal insulation properties of PET/aerogel blanket • Showed that by direct gelation of silica in non-woven matrix of PET under PH7, higher density PET/silica aerogel blanket was prepared having highly homogeneous and small spherical particle clusters with pores, which has positive effect on thermal and acoustic properties compared to the method of dipping PET non-woven matrix in the dispersion of silica hydrogel by varying PH condition in gelation process • PET/silica aerogel blanket provided higher thermal insulation value and lower sound absorption coefficient compared to PET non-woven fiber matrix and both were improved by increasing silica aerogel content
Coquard et al. [31]	<ul style="list-style-type: none"> • Performed numerical modeling of conductive heat transfer inside nano-structured silica-based materials using Boltzmann equation for nano-metric and microscopic scales and Fourier's law for macroscopic scale • Concluded that the insulating performances of the nano-structured silica based materials are mainly governed by the contact area of neighbouring silica particles and the aggregate compression leads to an increase of the mean number of contacts between particles and thus to an intensification of the heat transfer • Showed that the particle diameter affects the insulating performances more significantly at atmospheric pressure compared to 10 mbar partial vacuum since the Knudsen effect is directly related to this parameter
Wei et al. [30]	<ul style="list-style-type: none"> • Developed analytical model for conduction and radiation heat transfers using three-dimensional unit cell model • Showed that having lower density of xonotlite-type calcium silicate in xonotlite-aerogel composite lower k-value can be obtained • The effective thermal conductivity of the composite of the two materials decreases with the lower of pressure • The effective thermal conductivity can be greatly lowered having the composite of the two materials at an elevated temperature
J. B. Alvey [32]	<ul style="list-style-type: none"> • Degradation mechanisms of three different types of aerogel blankets were studied experimentally exposing them to elevated heat and humidity conditions • Moisture sorption, physical deformation, chemical change and humidity were introduced as the main factors of degradation in aerogel blankets

T. Xie et al. [33]	<ul style="list-style-type: none"> • Developed a computing procedure to calculate the thermal conductivity of silica aerogel composites doped with opacifiers considering heat conduction and thermal radiation • Showed that with small fiber and particle diameter, the extinction effect of additive on radiative heat transfer becomes more significant and the insulating performance becomes better • The best doped mass fraction of additive that corresponds to the lowest value of total conductivity was found to be the function of temperature • With increasing quantities of opacifiers or fibers, radiative heat transfer can be restrained and heat conduction can be increased • The poor insulating performance at high temperature is mainly due to the increased radiative heat transfer • Fiber orientation influences total conductivity
Zhao et al. [34]	<ul style="list-style-type: none"> • Developed a 2-D heat transfer model to investigate the relationship between the effective thermal conductivity and the actual composition and morphology of fiber-loaded aerogels using finite volume method • Showed that the effective thermal conductivity of the fiber-loaded aerogel can be reduced by reducing the fiber length-to-diameter ratio and the inclination angle and by moderately increasing the fiber volume fraction

As shown in Table 1-1, there is no compact analytical relationship, capable of predicting the effective thermal conductivity of a typical aerogel blanket material supported and verified thorough experimental studies that capture the ranges of low to high temperature conditions for different structured samples. Hence, in this research, one of the goals is developing an analytical model for predicting the thermal conductivity of aerogel blankets as a function of temperature, first in dry condition (RH=0%) and then the effect of humidity will be added to it. Material characterization has been performed to provide the input properties of the model, and experimental tests of thermal conductivity in various temperatures have been implemented for validating the model for two different commercially available samples.

1.2.2. Humidity Effect

Over the last few decades, it has been established that extensive failures in the performance of building components are often a result of thermal and moisture loads [35]. Temperature and humidity greatly affect the k-value of thermal insulations as well as indoor conditions [23]. There are several studies that investigated the mechanism of moisture diffusion into porous materials as well as the effect of this phenomenon on the variation of the k-value of conventional insulation materials. In the field of moisture diffusion analysis, Alvarez [36] experimentally studied different moisture diffusion models. He also developed an experimental apparatus to measure moisture transfer properties in porous materials under non-isothermal conditions. Stephenson [37] used a set of published results on glass fiber insulation to estimate

its thermal diffusion coefficient. His hypothesis was based on that moisture diffusion is related to the gradients of temperature and concentration at the same time. He concluded that the thermal vapor diffusion coefficient is approximately five times the coefficient for the diffusion due to the gradient of the vapor density.

Several studies have been performed on thermal performance of insulations in humid conditions. Thermal conductivities of brick [38], lime-based renders [4, 5], and stone wool [41] were reported to grow quite a few times when the measured values were compared in two different states: dry and water vapor saturated conditions. The effect of moisture content on the k-value of fibrous insulations was investigated in Ref. [42] and a relationship was presented to find the thermal conductivity at various moisture content at 24°C and 34°C. They showed that higher temperatures and higher moisture content was accompanied by higher thermal conductivity in fibrous insulations, which was more pronounced in lower density materials. Jerman and Cerny [43] showed that the thermal conductivity of all mineral wools increased significantly with increasing moisture content; which was from the range of 0.10–0.14 $\text{W}\cdot\text{m}^{-1}\cdot\text{K}^{-1}$ to 0.7–0.9 $\text{W}\cdot\text{m}^{-1}\cdot\text{K}^{-1}$ at saturation. Ochs et al. [44] modified the analytical model of Krischer and Kast [45] for the effective thermal conductivity of porous materials having moisture content by adding the concept of closed pore to the humidity model. They verified the model for expanded glass granules and expanded clay using experimental data of guarded heating plate device.

Based on the above, it can be concluded that: i) moisture transport in building materials is directly responsible for structural damage; and ii) neglecting the moisture dependence of thermal conductivity of insulations, specifically aerogel-based composites, in energy-related evaluations can lead to significant errors in heat loss calculations.

Because of the outstanding insulating properties of aerogel-based composites, they drew an immense interest in recent years for many applications. Table 1-2 summarizes the studies that have been performed on aerogel-based materials at humid conditions:

Table 1-2. Summary of the available studies on aerogel and aerogel-based composites at humid conditions.

Author(s)	Notes
Lakatos [46]	<ul style="list-style-type: none"> • Moisture induced degradation of thermal conductivity of aerogel blankets were studied experimentally and showed that thermal conductivity of the aerogel blankets can be increased significantly (approximately 20–40%) after wetting • Building Energy Simulations (BES) were evaluated to show the significant effect of moisture on increasing heat energy demand and primary energy demand using the experimental measurements of water uptake and thermal conductivity
Galliano et al. [47]	<ul style="list-style-type: none"> • Performed experimental and numerical study of transient hygrothermal properties of aerogel-based composites for internal retrofit of a wall • Showed that the boundary conditions, such as the surface heat resistance, are much more influential on heat flux or temperature in respect to material parameters
Stahl et al. [48]	<ul style="list-style-type: none"> • Highly insulating material using aerogel granules was developed • Thermal conductivity and water vapor transmission resistance were measured experimentally for the developed material • Concluded that liquid water enters the nano-pores of the aerogel granulate at humid conditions due to the high pressure damages partially the aerogel structure, remains trapped and will take a very long time to dry • Showed that the absence of cement binders causes a lower water vapour transmission resistance, which helps to avoid moisture accumulation on the cold side of inner insulation layers during summertime and condensation beneath the external rendering in wintertime
Ihara et al. [49]	<ul style="list-style-type: none"> • Experimentally showed that aerogel granules can have ~10% higher thermal conductivity after a moisture-aging test and concluded that a relatively long time may be required for such aging to occur under the actual conditions of aerogel applications • Suggested to consider moisture sources in installment specifications (e.g., condensation and rain) otherwise, an increased thermal conductivity should be considered in energy simulations
Wakili et al. [50]	<ul style="list-style-type: none"> • Performed in-situ measurement of temperature, humidity, and heat flux on aerogel-based plasters • Not able to reach a quasi-steady state condition in about a year • Combined transient heat and moisture transfer analysis was suggested as future work

As Table 1-2 indicates, in the literature, there is a lack of systematic theoretical and experimental investigation of k-value of aerogel-based materials at humid conditions. Therefore, there is a great need for developing analytical models that can accurately predict their thermal conductivity at various climatic conditions. The goal of this research is to identify the effect of moisture diffusion on thermal performance of aerogel blankets by presenting a combined experimental and theoretical study of heat and moisture transfer.

1.2.3. Mechanical Compression Effect

The higher R-value of building insulation corresponds to its better theoretical effectiveness. In many cases, instead of changing an insulation layer, it is economically desirable

to install an additional layer on top of the insulation that is already in place. Compression affects the nominal R-value of the insulators, so that the additional layer may result in a lower R-value, which is not desirable. Yarbrough et al. [51] studied the reduction of thermal resistance of loose-fill insulations due to mechanical compression and measured the thickness reduction as a function of applied load for samples of fiberglass batt, loose-fill fiberglass, loose-fill rock wool, and loose-fill cellulosic insulation. Their results showed that the low-density materials were affected the most, showing up to 40% thickness decrease under 0.14 kPa load. Also, they showed that reduction in thermal resistance under compression was greatest for the fiberglass insulations (~20% under 0.14 kPa load). Adams and Hust [52] investigated the reduction of thermal conductivity under compression for five common porous insulation products; cellulose, rock/slag wool, bonded and un-bonded glass fiber, and a glass fiber blanket. Graves and Yarbrough [53] measured the R-values of six commercially available fiberglass batts at their full thickness and compressed to 50% of full thickness, following ASTM C518 test methods. They observed that the decrease in thermal resistance during compression was greater for samples with higher density (compression to 50% of full thickness of higher density products reduced the R-value by 45%). Symons et al. [54] studied blanket form materials, e.g., low density fiberglass, sheep wool, and polyester fiber, as well as loose-fill form materials, e.g., cellulose fiber, sheep wool, and rock wool, following ASTM C518 standards. Their results showed that of the materials tested, the fiberglass blankets had the lowest thermal conductivity ($\sim 0.032 \text{ W}\cdot\text{m}^{-1}\cdot\text{K}^{-1}$), requiring less thickness (~ 80 mm) to achieve the target thermal resistance values of $2.5 \text{ m}^2\cdot\text{K}\cdot\text{W}^{-1}$ for a building in Australia. Kolich et al. [55] studied the thermal and physical properties of internal car insulation materials at -20 to 60°C and 0 to 60% compression. They determined specific heat of the samples, following ASTM E1269-05, and their volume density using ASTM C302-95. They also correlated increases in apparent thermal conductivity of uniform porous materials with increasing density, and found that the apparent thermal conductivity of laminated materials (e.g., foam plastic-leader) decreased with increasing density, which was caused by variation in the shape of the pores.

To the best of our knowledge, there are only a few limited studies on the relationship between thickness, compression, deformation, and thermal performance of aerogel-based composite insulation materials. A summary of available studies on aerogel composites is presented in Table 1-3.

Table 1-3. Summary of available studies on thickness or density of aerogel-based composites.

Author(s)	Notes
Cuce et al. [56]	<ul style="list-style-type: none"> • Investigated the optimum thickness of aerogel blankets to maximize energy saving and thermal comfort and determined the dependency of annual energy use on insulation thickness • Concluded that aerogel-based thermal super-insulations provide remarkably slimmer constructions and larger living spaces in buildings compared to the conventional insulations as well as providing 55.2% reduction in CO₂ emissions for insulated cavity walls • Showed that the aerogel insulation can be considered for colder climates and for the investments with longer lifetime
Gupta and Ricci [57]	<ul style="list-style-type: none"> • Fabricated aerogel/epoxy composites • Experimentally studied the composites (density of 980 and 1070 kg·m⁻³) under compressive loads (0-120 MPa) • Observed some cracks but no strength loss at 25% compressive strain
Bardy et al. [58]	<ul style="list-style-type: none"> • Tested samples of prototype and product-line aerogel insulating blankets for thermal conductivity and compressive strain at incremental loads up to 1.2 MPa • Found that the prototype sample has higher resistance under compression and recovers to its original thickness upon decompression
Duoqi Shi et al. [59]	<ul style="list-style-type: none"> • Fabricated ceramic-fiber-reinforced SiO₂ aerogel • Investigated the composite properties under compression (up to 1.5 MPa for in-plane and 16 MPa for out-of-plane compression) at high temperatures (up to 900°C) • Found that in-plane Young's modulus and fracture stress increase with temperature, but out-of-plane modulus decreases with temperature • Showed that the out-of-plane property does not change with loading rates and viscous flow at high temperature was found to cause in-plane shrinkage, and both in-plane and out-of-plane properties change
Wu et al. [60]	<ul style="list-style-type: none"> • Fabricated multilayer fiber-reinforced aerogel composites using glass fiber and SiO₂ aerogel • Analytically studied the effect of fiber alignments on the compressive and bending strengths and thermal conductivity of the composites • Demonstrated a feasible way to improve the mechanical strengths but still maintain the low thermal conductivity of the aerogel composites via impregnating multilayer aligned fibers into aerogels

Our literature review indicates that the effect of compression on the thermal performance and structural deformation of aerogel blankets has not been thoroughly studied yet. Silica aerogel can crack and separate from the fibrous matrix, which affects the thermal resistance of the aerogel blanket insulation. As such, the focus of this research is to measure the thermal performance of two types of aerogel blanket samples under compression and after repeated mechanical load cycling. Additionally, a mechanistic analytical model is developed, following a unit cell approach, for predicting the deformation of the aerogel blankets as a function of compressive mechanical load. Bending of fibers is considered as the main deformation mechanism at the unit cell level and the overall blanket deformation is calculated from the summation of the deformations of all

the layers. Employing the proposed model, a compact relationship between compressive strain and applied load (stress) is presented, which is verified using the experimental data that can be employed in predicting the deformation of any fibrous insulation material at a particular density.

1.2.4. Lack of the Literature

The previous section on literature review indicated that the focus of the pertinent research in the area of the thermal insulation materials has been mostly on conventional insulations, with some experimental studies on aerogel and aerogel-based insulation materials. There is not an in-depth study to investigate the aerogel blanket insulation material thermal performance. The present study aims to address this shortcoming by investigating the effect of realistic operating conditions, e.g., temperature, humidity, and also mechanical compression on thermal performance of aerogel blankets, in order to be used as an efficient building/greenhouse envelope. In our quest to study this material, mathematical models are developed and supported by material characterization, then verified using experimental studies. These models can be utilized in predicting the actual thermal performance of buildings, design and development in construction industry and design optimization in aerogel blanket manufacturing process with the target of cost reduction.

Chapter 2.

Thermal Analysis of Aerogel Blankets

The porous nature of aerogel blanket makes it necessary to define an effective thermal conductivity, to predict its k-value under various operating conditions and optimize its thermal performance in new designs. In general, for aerogel blankets, there are nano/meso-scale pores and matrix, as well as micro-scale additives, such as fibers and opacifier. The heat transfer modes include gas conduction, solid conduction, and thermal radiation. These multi-scale topology structures make multi-mode heat transfer to be enormously complex. The purpose of this study is to provide an analytical model for calculating the effective thermal conductivity of silica aerogel composite insulating materials in which heat conduction and thermal radiation are taken into account simultaneously. In such materials, two components are distributed randomly (fiber and aerogel particles), either component may form continuous heat conduction pathways, depending on the relative amounts of the components, and therefore this structure is unbiased towards its components and an effective property can be defined to describe the behavior of the material. The properties of these type of structures such as effective thermal conductivity has been modelled well by the Effective Medium Theory (EMT) [61]–[63], [64][65],[60],[66], [30], [21]. In this theory, a unit cell is a small geometrical block that can describe the salient properties of the medium and is assumed to be repeated throughout the structure. Using the observations of Aspek Explorer SEM imaging, the proposed unit cell is assumed to be a ‘packed bed’ of spherical aerogel particles with more than 90% porosity and a solid cylindrical fiber at the center. A new analytical model for predicting the thermal conductivity of aerogel blankets as a function of temperature and relative humidity is proposed and validated for two types of aerogel blankets. Moreover, a parametric study is performed to investigate the effect of key parameters on the effective thermal conductivity of aerogel blankets, which is presented in the results and discussion section. The results of this chapter is also published in the International Journal of Heat and Mass Transfer and Journal of Building Engineering[67],[68]. The experimental studies were all performed by the author of the thesis as well as developing the analytical model. In defining the geometry of the problem for the modeling part the co-authors have had major contributions.

2.1. Mechanisms of Heat Transfer in Insulations

2.1.1. Conduction

Thermal conductivity is a measure of the amount of heat that flows through a material by conduction heat transfer. The measurements are based on Fourier's law of heat conduction, which is showed in Eq. (1) for a 1-D heat transfer problem. This equation is valid only when the thermal conductivity can be assumed constant.

$$\dot{q} = -k \frac{dT}{dx} \quad (1)$$

where \dot{q} is heat transfer per unit area ($\text{W}\cdot\text{m}^{-2}$), T is the temperature (K or $^{\circ}\text{C}$), x is the direction of heat flow (m), and k is the thermal conductivity coefficient ($\text{W}\cdot\text{m}^{-1}\cdot\text{K}^{-1}$). Conduction occurs in solids, liquids, and gases. Gases have lower thermal conductivity than solids or liquids, therefore, for thermal insulations, where minimum heat transfer is desirable, small volume fraction of solid material and large volume fraction of gas, such as air, is required.

2.1.2. Convection

If conduction was the only pathway of heat transfer, then obviously, the best for insulation materials would be to fill large voids with low conductivity gases. However, due to the motion of gas molecules, convective heat transfer also plays an important role in thermal insulation performance. Gas particles in contact with a heat source participate in a conductive heat transfer and then move away due to buoyancy or other forces, from the original location until the next collision, where further conduction takes place. The solution to this is to break up the volume of gas pore into a large number of small voids until the contribution of convection to the overall heat transfer becomes negligible [28], [34], [69].

2.1.3. Radiation

Thermal radiation is the heat transferred through electromagnetic waves and generally is defined as following:

$$\dot{q} = \varepsilon \sigma T^4 \quad (2)$$

where ε is the emissivity and $\sigma=5.7\times 10^{-8}$ W·m⁻²·K⁻⁴ is the Stefan-Boltzmann constant. The emissivity is an indication of how opaque the material is to thermal radiation. Although both conduction and convection are driven by a temperature difference, radiation is driven by a difference of the fourth power of (absolute) temperature (K). This means that for low temperatures, radiation can be comparable to the other modes of heat transfer, but at higher temperatures, radiation becomes much more dominant. The method of calculating the contribution of radiation heat transfer in the apparent thermal conductivity of aerogel blankets will be discussed in this work.

2.1.4. Effective Thermal Conductivity

Thermal insulation is designed to retard the heat flow from one region to another; the mentioned heat transfer takes place through a combination of conduction (gas and solid) and radiation. Usually, the measurement of pure conduction is challenging, therefore, measured thermal conductivities of insulating materials include all modes of heat transfer and it is called “effective” thermal conductivity. For modeling the heat transfer, thermal resistance network, which is the electric circuit analogy, is typically being used. The thermal resistances are called R-values (m²·K·W⁻¹) and defined using the effective thermal conductivity as followed:

$$R = \frac{t_s}{k_{eff}} \quad (3)$$

where t_s is the material thickness (m).

Aerogel blankets have low thermal conductivity, due to (1) the high porosity, the small fiber-fiber contacts, and the very long solid conduction path through the aerogel skeleton, which reduce the solid thermal conduction [1,2]; (2) the restricted gas mean free path with restricted molecular collisions in the nano-pores, which reduces the gaseous thermal conduction [1,2,30]; and (3) the large extinction coefficient due to the fibers, which reduce the radiative heat transfer.

2.2. The present Model

The proposed geometrical model for the unit cell approach is shown in Figure 3. It consists of two domains: a rigid solid cylindrical fiber; and a spherical aerogel packed bed around it, both into a noticeable void space in which heat flows in the z-direction (along the sample thickness).

Temperature gradients in the x and y direction are negligible (adiabatic boundary condition) and constant temperature is assumed at $z=0$ and $z=l_u$ to be able to solve the problem analytically. Therefore, heat transfer is only solved in the z-direction.

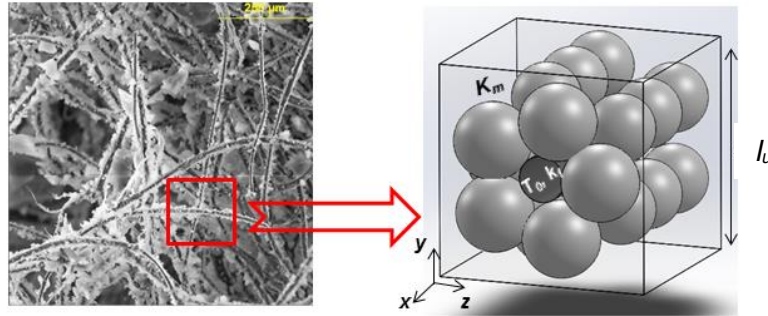


Figure 3. Proposed unit cell for aerogel blanket geometrical modeling.

The assumptions used in the model development are listed below:

- Steady-state one-dimensional heat transfer in the medium;
- Negligible natural convection due to small pore sizes (<4 mm); one can calculate the Rayleigh number ($Ra = \frac{\beta g}{\nu \alpha} (T_h - T_c) d_p^3$ in which d_p is the average pore diameter (m), g is gravitational acceleration ($m \cdot s^{-2}$), T_h and T_c are temperature of hot and cold surfaces (K), α is thermal diffusivity ($m^2 \cdot s^{-1}$), ν kinematic viscosity ($m^2 \cdot s^{-1}$) and β thermal expansion coefficient (K^{-1}) based on the average pore size (See appendix A) to find $Ra \sim 10^{-3}$, which is significantly lower than 1708, that is the threshold for natural convection to be a considerable contributing mechanism in enclosures [30];
- Smooth spheres and fiber surfaces, *i.e.*, no roughness between contacting spheres and the fiber;
- Simplified fiber orientation and morphology to calculate the solid thermal conduction; and
- No heat generation source in the medium.

Therefore, the unit cell modeling consists of two parts: 1) Solid and gas (fluid) conduction heat transfer modeling of the cylinder and its surrounding medium, and 2) Radiation heat transfer modeling of the unit cell. Presented in Eq. (4), solid-gas conduction as well as radiation are modeled as two parallel paths of one dimensional heat transfer in aerogel blankets [70], which for both of them, coefficients are defined and modeled in the following sections. In thermal insulation materials the through plane thermal conductivity is the dominant factor in heat transfer as there are constant boundary conditions on both sides of the material and from now on by “the effective thermal conductivity” the author means “the through plane thermal conductivity”.

$$\dot{Q}_{tot} = k_{eff} A \frac{dT}{dz} = \dot{Q}_{cond.} + \dot{Q}_{rad.} \quad (4)$$

2.2.1. Conduction heat transfer

Conduction heat transfer in the unit cell is a function of the fiber and medium thermal conductivities. Following [71], a compact relationship for thermal conductivity of an infinite cylinder (fiber) in an infinite medium (aerogel packed bed) with a linear temperature gradient can be developed. The summary of the equations that lead to the final relationship for conduction heat transfer is presented below:

$$\frac{T}{T_{fiber}} = \left[1 - \frac{k_{fiber} - k_m}{k_{fiber} + k_m} \left(\frac{r_{fiber}}{r} \right)^2 \right] Z$$

$$Z = \frac{z}{r_{fiber}} \quad (5)$$

$$z = r \cos(\theta)$$

where k_{fiber} and k_m are thermal conductivities of the fiber and its surrounding medium, respectively and r_{fiber} is the fiber radius (m). l_u is the unit cell length calculated using the following equation:

$$\varepsilon_b = \frac{V_{void}}{V_{tot}} = \frac{(l_u^2 - \pi r_{fiber}^2) \varepsilon_m}{l_u^2} \quad (6)$$

Here, V_{void} is the volume of the unit cell empty spaces (m^3), V_{tot} is the total volume of the unit cell (m^3), and ε_b and ε_m are blanket and medium porosities, respectively. In this study, blanket porosity is measured by mercury intrusion porosimetry (MIP) and the porosity of aerogel packed

bed exists in the literature [72] as the medium (which is 95%), so that unit cell length has been calculated afterwards using Eq.(6).

Having the temperature distribution in the proposed unit cell, the effective conduction heat transfer coefficient of the blanket can be calculated using Eq.(7):

$$k_{cond.} = \frac{k_m \left. \frac{\partial T}{\partial z} \right|_{\frac{l_u}{2}}}{\frac{\Delta T \left|_{\frac{l_u}{2}}^2}{l_u}} \quad (7)$$

Simplifying Eq.(7) yields a compact relationship for the contribution of conduction heat transfer in the effective thermal conductivity of the blanket.

$$k_{cond.} = \frac{k_m [4\sqrt{2}(\frac{r_{fiber}}{l_u})^2 (k_{fiber} - k_m) + 1.77(k_{fiber} + k_m)]}{-4\sqrt{2}(\frac{r_{fiber}}{l_u})^2 (k_{fiber} - k_m) + 1.77(k_{fiber} + k_m)} \quad (8)$$

Thermal conductivity of the porous medium around the fiber containing dry air and aerogel particles

In Eq.(8), k_m is the aerogel packed bed (as the medium around the fiber) thermal conductivity, which consists of conduction of fluid inside the pores and solid conduction through spherical aerogel particles. Different approaches can be used to obtain the thermal conductivity of a bed of spheres filled with a fluid, which can be categorized into two main divisions: numerical and analytical approaches. Buonanno and Carotenuto [73] used a three-dimensional Finite Element Analysis (FEM) model to calculate the thermal conductivity of simple cubic and body center cubic packed beds. Buonanno *et al.* [74][75] measured the effective thermal conductivity of uniformly-sized rough stainless steel spheres. Their FEM numerical modeling results are in good agreement with the experimental data. Analytical models for calculating the effective thermal conductivity of the packed beds of uniformly sized spheres have been established by Ogniewicz and Yovanovich [76] and Turyk and Yovanovich [77] and verified with experimental data. Bahrami *et al.* [78] also developed a model for predicting the effective thermal conductivity of a packed bed of rough spheres and implemented contact mechanical and thermal analyses to present the results as a compact relationship. Wei *et al.* [79] evaluated the thermal conductivity of silica

aerogel powder as an insulation material. They measured gaseous conductivity values from very low pressures up to the ambient pressure and showed its dependence on pressure. In this study, Zehner-Schlunder's [66] modified model for spherical packed beds has been followed to calculate the thermal conductivity of the medium. They assumed that heat transfer occurs through three parallel paths, as they showed in their unit cell: i) the fluid region (air in dry condition (RH=0%) with $Kn < 0.1$), ii) solid and fluid region and iii) the solid region. Therefore, following [66], the thermal conductivity of the medium is given by Eq.(9):

$$k_m = \left(1 - \frac{1}{R'^2}\right)k_f + \left(\frac{1-r_s^2}{R'^2}\right)k_{fs} + \left(\frac{r_s}{R'}\right)^2 k_s \quad (9)$$

where k_{fs} is the equivalent thermal conductivity of the region that consists of fluid and solid phases, R' is the radius of packed bed unit cell, r_s represents the radius of contact area between the spheres at $r=r_s$ and $z=1$, and k_f and k_s are the fluid and solid (silica aerogel) thermal conductivities, respectively. The unit cell radius, R' , is obtained from Eq.(10), which is an empirical relationship, in which ε_m is the medium effective porosity, and radius of the contact area, r_s , is determined by Eq.(11); where α is the deformed factor to show the area contact between the spheres. This parameter is difficult to measure experimentally and in this work it is used as a fitting parameter. The value assumed for α is 0.1.

$$\frac{1}{R'^2} = \sqrt{(1-\varepsilon_m)} \quad (10)$$

$$r_s = 1 - \frac{1}{(1+\alpha)^2} \quad (11)$$

Assuming that the thermal resistances of the solid and fluid phases are in series with respect to the temperature gradient, the resulting relationship for k_{fs} is:

$$\frac{k_{fs}}{k_f} = \frac{2}{1-\zeta} \left(\frac{1}{1-\zeta} \ln\left(\frac{1}{\zeta}\right) - 1 \right) \quad (12)$$

ζ is the ratio of fluid thermal conductivity to solid thermal conductivity:

$$\zeta = \frac{k_f}{k_s} \quad (13)$$

Here, the model is modified to include the gas rarefaction effects (Knudsen effect) to show the deviation from the classical theory when gas flows through a micro channel. Therefore, k_f is defined as following:

$$k_f = \frac{k_{g0}}{1 + 2\xi Kn} \quad (14)$$

k_{g0} is the gaseous conductivity at STP ($p=1$ atm and $T= 298$ K), which is calculated for dry air as below [44]:

$$k_{air} = 0.00243 + 7.8421 \times 10^{-5}(T + 273.15) - 2.0755 \times 10^{-8}(T + 273.15)^2 \quad (15)$$

ξ is a constant, specific to the gas in the pores. It is calculated from the gas accommodation coefficient, α_T , and the specific heat ratio of gas, $\gamma=C_p/C_v$.

$$\xi = \left(\frac{9\gamma - 5}{2\gamma + 1} \right) \left(\frac{2 - \alpha_T}{\alpha_T} \right) \quad (16)$$

For dry air, α_T is 0.8 and γ is 1.4 at room temperature [80]. Kn is the Knudsen number defined as $Kn=\Lambda_m/d_p$, d_p is the mean pore size of the blanket in this work (See Appendix A), and Λ_m is the mean free path of gas molecules in free space, calculated as Eq.(17):

$$\Lambda_m = \Lambda_{m0} \frac{P_0}{P} \frac{T}{T_0} \quad (17)$$

where Λ_{m0} is in standard condition (69 nm for air at ambient pressure and 298 K [81]).

Thermal conductivity of the porous medium around the fiber at humid conditions

Actual thermal conductivity of insulation materials is subject to change over time under various environmental conditions. Particularly, insulations may degrade due to moisture absorption or condensation when they are exposed to humidity. Having the proposed unit cell in Section 2.2.1, in a humid environment, pores of the aerogel blanket unit cell would be partially filled with water vapor accompanying some adsorbed water. Therefore, the unit cell should be

modified as shown schematically in Figure 4. This part presents an investigation of aerogel blankets thermal conductivity (k -value) in humid conditions at transient and steady-state regimes.

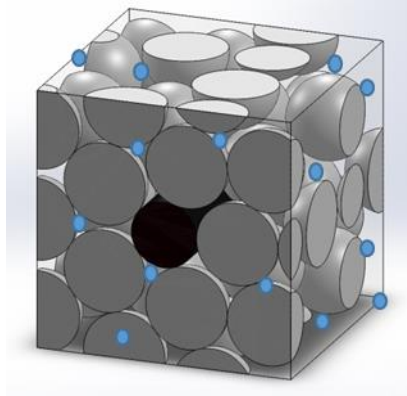


Figure 4. Schematic of the moisture distribution inside the pores of the proposed unit cell; small blue circles depict adsorbed water.

When an aerogel blanket is placed in a humid environment, it takes hours for moisture to diffuse from the surface of the material to its depth and establish no concentration gradient inside the pores. The reason is that the material shows “resistance” against diffusion of humidity into the pores as well as providing a “capacity” to store moisture inside the pores. This phenomenon can be described using a well-established resistance-capacitance (RC) model that employs a representative electric circuit to simulate the mass diffusion in aerogel blankets [82].

Modeling a mass transfer in a porous material using an RC model requires finding its equivalent electric circuit. Once the equivalent resistance and capacitance are defined and the circuit is set up, based on the analogous electrical network, the mass transfer phenomena can be modeled using the solution to the electric circuit [83]–[86]. This method is widely used in numerous industrial applications such as fuel cell systems [87]–[90]. The proposed zero-dimensional RC circuit (lumped system) for aerogel blanket porous medium is shown in Figure 5 and the equivalent parameters are shown in Table 2-1.

Table 2-1. Table of equivalent parameters in electrical and mass transfer systems.

Electrical system	Mass transfer system
Current (I , ampere = coulomb/sec)	Water flow rate (\dot{m}_w , kg/sec)
Potential difference (V , volts)	Water vapor concentration (c_w , kg/m ³)
Electron charge (Q , coulombs)	Moisture content (m_w , kg)
Electric capacitance (C , Farad=coulomb/volt)	Mass storage capacitance, (C , m ³)
Electric resistance (R , Ohm= volts·s/coulomb)	Diffusion resistance, (R , s/m ³)

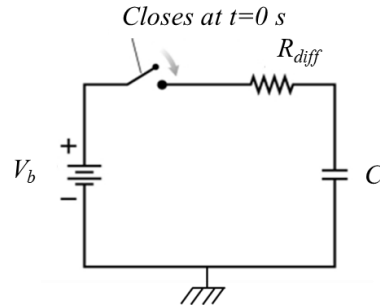


Figure 5. Zero-dimensional (lumped) RC model of aerogel blanket insulation material in humid conditions.

In Figure 5, once the switch is closed at $t=0$ s, the moisture diffuses into the material and fills up the pores, *i.e.* electrons charge the capacitor until it is fully charged and then the current becomes zero. The resistance against the diffusion of moisture (R_{diff}) is defined following Fick's law and is shown in Eq.(18):

$$R_{diff} = \frac{t_s}{D \cdot A_s} \quad (18)$$

where D is the diffusion coefficient of moisture; and t_s and A_s are thickness and the cross sectional area of the sample, respectively.

Also, C shows the mass storage capacitance of the system that can be calculated using the maximum charge that a capacitor can hold (Q_{max}) and the voltage of the source (V_b) [91]. In this study, the moisture content of the material (m_w) and moisture concentration (c_w) in the porous medium are equivalent to the electron charge (Q) and potential difference (V) in the electrical system, respectively. Hence, having the maximum moisture content of the aerogel blanket samples, which has been measured as will be discussed in section 2.3.2, the mass storage capacitance can be calculated using Eq.(19):

$$C = \frac{Q_{\max}}{V} = \frac{m_{w_max}}{c_w} \quad (19)$$

where m_{w_max} is the weight of the moisture in the sample at steady-state condition. The water concentration, c_w ($\text{kg}\cdot\text{m}^{-3}$), is also calculated at each specific RH (relative humidity) by assuming water vapor is an ideal gas:

$$c_w = \frac{M_w \cdot P_{sat}}{R \cdot T} (RH) \quad (20)$$

where M_w is the molecular weight of water ($18.01 \times 10^{-3} \text{ kg}\cdot\text{mol}^{-1}$) and R is gas universal constant ($8.31451 \text{ J}\cdot\text{mol}^{-1}\cdot\text{K}^{-1}$). P_{sat} is the saturation pressure of water vapor (Pa) calculated from Eq.(21)

$$P_{sat} = 610.78 \exp\left(\frac{17.27T + 4717.30}{T}\right) \quad (21)$$

Therefore, moisture content of the samples over time is calculated using Ohm's law and voltage law for a circuit of series capacitor and resistor, according to Eq.(22):

$$m_w = m_{w_max} [1 - e^{-t/\tau}] \quad (22)$$

where τ is the time constant of the system and is calculated as follows:

$$\tau = R_{diff} \cdot C \quad (23)$$

Predicting the moisture content of aerogel blanket materials over time enables us to predict their k-value at any given time under any T and RH condition.

The adsorbed water, depicted in Figure 4, is assumed to be distributed evenly throughout the medium of the unit cell due to not having enough information about the water distribution in the material at high humidity. More importantly, the results showed that the proposed model is able to predict the data successfully. Considering that in humid conditions pores include humid air (known RH) as well as liquid water, the medium thermal conductivity of the unit cell, k_m , should be re-defined accordingly:

$$k_{m_humid} = (1 - \sqrt{(1 - \varepsilon_{m_humid})})k_{f_humid} + \sqrt{(1 - \varepsilon_{m_humid})}(1 - r_s^2)k_{fs_humid} + \sqrt{(1 - \varepsilon_{m_humid})}r_s^2k_s \quad (24)$$

where k_{m_humid} is the medium thermal conductivity at humid conditions. k_{f_humid} is estimated from Maxwell-Eucken model for calculating the thermal conductivity of the mixture of fluids; i.e. humid air as the gas phase (k_g), and water (k_w) as the liquid phase [92]:

$$k_{f_humid} = k_w \frac{2k_w + k_g - 2(k_w - k_g)\varphi_g}{2k_w + k_g + (k_w - k_g)\varphi_g} \quad (25)$$

In Eq.(25), φ_g is the volume fraction of humid air inside the pores, calculated using Eq.(26) :

$$\varphi_g = 1 - \varphi_w \quad (26)$$

where φ_w is the volume fractions of water inside the pores, which can be calculated having moisture content of the samples over time, as is shown in Eq.(27) and Eq.(28). It should be noted that the aerogel materials are super hydrophobic and do not adsorb moisture, i.e. water and humid air fill up the pores or gradually get attached to the surfaces of the pores.

$$\varphi_w(t) = \frac{u(t)}{\varepsilon_b \cdot V_{dry}} \quad (27)$$

$$u(t) = \frac{m_w(t)}{\rho_w} \quad (28)$$

where u is the volume of the water inside the sample (m^3), and m_w is the moisture content of the sample, (kg) both are changing over time. Moisture content modeling over time has been already discussed. ρ_w is the density of water ($kg \cdot m^{-3}$) and V_{dry} is volume of the dry blanket.

Thermal conductivity of water is estimated using Eq.(29) [44] :

$$k_w = 0.557 + 0.0022(T + 273) - 1.051 \cdot 10^{-5}(T + 273)^2 + 1.081 \cdot 10^{-8}(T + 273)^3 \quad (29)$$

To calculate the humid air thermal conductivity, Eq.(14) is used and k_{g0} is defined as thermal conductivity of the ideal mixture of water vapor and air at standard condition. It can be calculated knowing the volume fraction of water vapor and air as shown in Eq.(30):

$$k_{g0} = x_v k_v + (1 - x_v) k_{air} \quad (30)$$

where x_v is the volume fraction of water vapor calculated having RH and T as follows:

$$x_v = RH \frac{P_{sat}}{P_{amb}} \quad (31)$$

where P_{amb} shows the ambient pressure (1 atm). Since volume fraction of vapor is an insignificant value in the considered T and RH, in Eq.(30), the first term is negligible ($x_v k_v \ll (1 - x_v) k_{air}$), and k_{g0} can be estimated just by knowing the dry air thermal conductivity ($k_{g0} \approx k_{air}$) (Eq.(15)).

The remaining parameter in Eq.(24), k_{fs_humid} , is calculated having all the defined parameters:

$$k_{fs_humid} = \frac{2k_{f_humid}}{1 - \frac{k_{f_humid}}{k_s}} \left(\frac{1}{1 - \frac{k_{f_humid}}{k_s}} \ln\left(\frac{1}{\frac{k_{f_humid}}{k_s}}\right) - 1 \right) \quad (32)$$

Moisture supplement for the thermal conductivity (Z constant)

Effect of the diffused moisture on thermal conductivity of an insulation material is typically reported by the percentage of the difference in wetness levels. According to Ref.[46] and [93] a simple approximation can be used to find the aerogel blanket moisture supplement for the thermal conductivity (Z constant) following Eq.(33):

$$k_{eff_humid} = k_{eff_dry} (1 + (\omega Z / 100)) \quad (33)$$

where k_{eff_humid} and k_{eff_dry} are the thermal conductivity of the humidified sample and not humidified sample (dry sample), respectively. ω is the non-dimensional moisture content (kg/kg) calculated using Eq.(34) following the method to be described in section 2.3.2:

$$\omega(\%) = \frac{m_{wet} - m_{dry}}{m_{dry}} \times 100 \quad (34)$$

Z is the material constant and demonstrates the moisture supplement for the thermal conductivity.

2.2.2. Radiation heat transfer

A portion of heat transfer through aerogel blankets is due to radiation. When a material is optically thick (optical thickness (OT) $\gg 1$), such as thermal insulation materials, radiation travels only a short path before being scattered or absorbed and heat transfer is mainly dependent on the mean free path of photons. The optical thickness of an insulation material is defined as the extinction coefficient times the physical thickness of the material. There are three regions of optical thickness [94]: OT $\ll 1$ which is a transparent material, (OP) $\ll 1$ which is an optically thin material and OP $\gg 1$ which is an optically thick material. The optical thickness for a sample of CZ aerogel blanket with a 10 mm thickness and extinction coefficient of 4014 m⁻¹ is 40.14. Therefore, the material is optically thick, which means that local intensities will not be influenced by distant elements. In other words, intensities from far away elements will be diminished if many radiative interactions occur in the intervening distance to the element of concern. The total number of radiative interactions is equal with the optical thickness. In this situation, radiative heat transfer can be modeled using the Fourier's heat conduction law, called the diffusion approximation method [95]. The requirement for applying diffusion approximation method is that firstly the temperature gradient is substantially small over the mean free path of radiation, and secondly the temperature level of the media is equivalent to that of its surroundings so that intensities from distant elements are insignificant. Assuming a temperature gradient of 100°C across an aerogel blanket of 10 mm thick, and a characteristic diameter of 100 μm, the result is a temperature gradient of 1°C per pore diameter. In terms of absolute temperatures, this is an insignificant gradient and diffusion approximation method is valid for such a material."

In this method, the corresponding thermal conductivity coefficient, k_{rad} , can be found from Eq.(35) [95]:

$$k_{rad} = \frac{16\sigma T^3}{3K_R} \quad (35)$$

In this equation, σ is Stefan-Boltzmann constant ($W \cdot m^{-2} \cdot K^{-4}$) and $K_R (m^{-1})$ is the Rosseland mean extinction coefficient of the blanket. The extinction coefficient shows the deterioration rate of the radiation intensity passing through the material and is the inborn feature of material. The Rosseland mean extinction coefficient is obtained from Eq.(36) at 25°C [95]:

$$\frac{1}{K_R} = \frac{\int_0^{\infty} \frac{1}{\beta_\lambda} \frac{\partial e_{b\lambda}}{\partial T} d\lambda}{\int_0^{\infty} \frac{\partial e_{b\lambda}}{\partial T} d\lambda} = \int_0^{\infty} \frac{1}{\beta_\lambda} \frac{\partial e_{b\lambda}}{\partial e_b} d\lambda \quad (36)$$

In this equation, λ shows wavelength (m), which in this study the range of 2.5– 40 μm was chosen for to cover the infrared region of the spectrum since we are concerned with the absorption of light in the infrared region of the electromagnetic spectrum where more than 50% of thermal radiation lies in. T is the medium temperature, e_b is the blackbody emissive power, $e_{b\lambda}$ is the spectral black body emissive power, and β_λ is the spectral extinction coefficient. For black bodies, the monochromatic emissive power was derived by Planck by introducing the quantum concept for electromagnetic energy as:

$$e_{b,\lambda} = \frac{2\pi hc^2}{\lambda^5 (\exp(hc / K_s T \lambda) - 1)} \quad (37)$$

where c is the speed of light ($2.97792458 \times 10^8 \text{ m} \cdot \text{s}^{-1}$), h is the Plank's constant ($6.62607004 \times 10^{-34} \text{ J} \cdot \text{s}$) and K_s is the Boltzmann constant ($1.38064852 \times 10^{-23} \text{ J} \cdot \text{K}^{-1}$). The spectral extinction coefficient, which represents the scattering and absorption, can be found either by analytical models based on the type and morphology of fibers or from experimental methods. The experimental approach uses the measured transmittance spectrum from a FTIR spectrometer to calculate the spectral extinction coefficient. The spectral extinction coefficient for a thin sample can be obtained using Beer's law [95]. Beer's law states that the magnitude of intensity in a given direction will change as a result of absorption and scattering events, which summarily define extinction events, as it moves along that direction in a medium of thickness t_s [94].

$$\beta_\lambda = -\frac{\ln(T_{n\lambda})}{t_s} \quad (38)$$

$T_{n\lambda}$ is the spectral transmittance ($\log(T_{n\lambda}\%) = 2 - \text{absorbance}$) and t_s is the thickness of the sample (m). In this study, the spectral transmittance was measured for two types of aerogel blankets using FTIR spectroscopy, which will be explained in details in section 2.3.

Finally, presented in Eq.(39) is the final relationship for the effective thermal conductivity of the aerogel blanket at dry or humid conditions obtained by superposition of the conduction and radiation thermal conductivities as following [70] (See Appendix D for derivation of this equation):

$$k_{eff} = k_{cond.} + k_{rad.} \quad (39)$$

2.3. Experimental study

In this research, samples of aerogel blanket produced by two manufacturers, Aspen Aerogel Inc. and Cabot Aerogel Corp., are investigated. Table 2-2 shows the specifications of the samples in terms of what manufacturers reported and what were tested in this study.

Table 2-2. Aerogel blanket samples specifications

Manufacturer Data [60, 61]						
Sample	Provider	Thickness	Density*	Fiber composition	Powder material	Thermal* Conductivity
Cryogel® Z (CZ)	Aspen Aerogel	10±0.5 mm	130 kg·m ⁻³	Polyester/ fiber glass	Silica (SiO ₂)	0.014 W·m ⁻¹ ·K ⁻¹
		5±0.5 mm				
ThermalWrap™ (TW)	Cabot Corp.	8±0.5 mm	70 kg·m ⁻³	Polyester and polyethylene	Silica (SiO ₂)	0.023 W·m ⁻¹ ·K ⁻¹
		5±0.5 mm				
Measured Values						
Sample	Particle diameter	Standard deviation	Fiber diameter	Standard deviation	Porosity	Extinction coefficient
CZ	10 μm±5 μm		12 μm±3 μm		91%±7%	4014 m ⁻¹
TW	13 μm±4 μm		9 μm±2 μm		79%±7%	3165 m ⁻¹

*At room temperature

The values of fiber and aerogel particle diameter as well as average pore size are average of 100 measurements from the taken SEM images of both samples. The SEM images were processed using Image J software. Thickness of the samples was measured by a ruler that had uncertainty of ±0.5 cm. The manufacturer data sheets indicate that CZ has more aerogel content in a unit of volume and larger fiber diameters, compared to TW, which results in having higher density.

The extinction coefficients of both aerogel blanket samples were determined from their spectral transmittance, which are shown in Figure 6 (a) and (b). The spectral transmittance was measured using a Fourier Transform Infrared (FTIR) spectroscopy using FTIR spectrometer (Model Shimadzu IRPrestige-21) for the wavelength range of 2.5–40 μm . The extinction coefficients were subsequently calculated by using Eq.(36). The peaks at $\sim 1060\text{ cm}^{-1}$ and $\sim 460\text{ cm}^{-1}$, in both plots of Figure 6, are associated with the Si–O–Si asymmetric bond stretching vibration, and Si–O–Si bond bending vibration, respectively, which means the successful chemical gelation in aerogel synthesis. The peaks occurring at $\sim 860\text{ cm}^{-1}$ are due to Si-CH₃ bonds. The surface modification/solvent exchange in the process of aerogel synthesis could be confirmed by the observation of these peaks. The small transmittance peaks at $\sim 3600\text{ cm}^{-1}$ and $\sim 3100\text{ cm}^{-1}$ are due to the hydroxyl group at the end of gel network or residual water molecules [98].

The porosities of the samples were measured by the MIP method using a mercury intrusion porosimeter (AutoPore IV, Micromeritics Instrument Corporation).

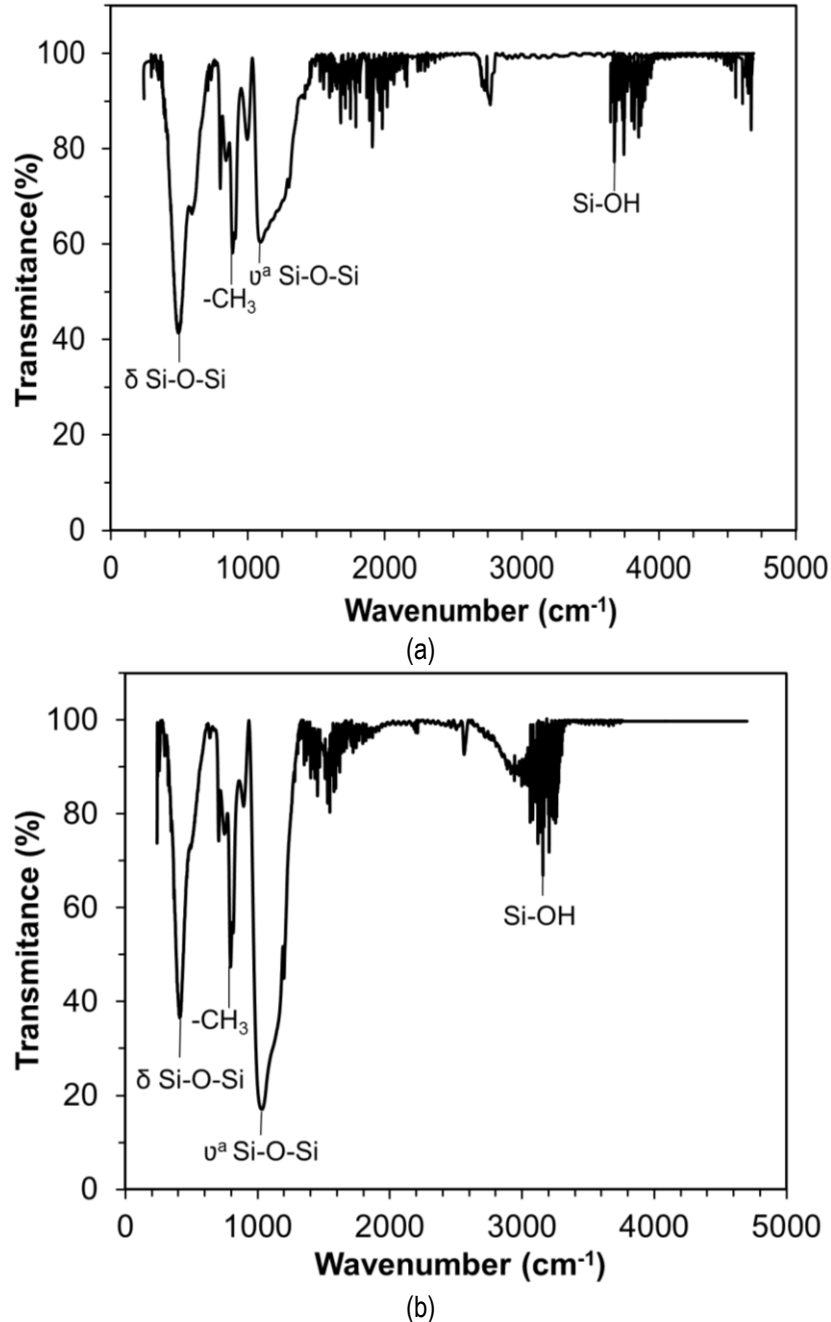


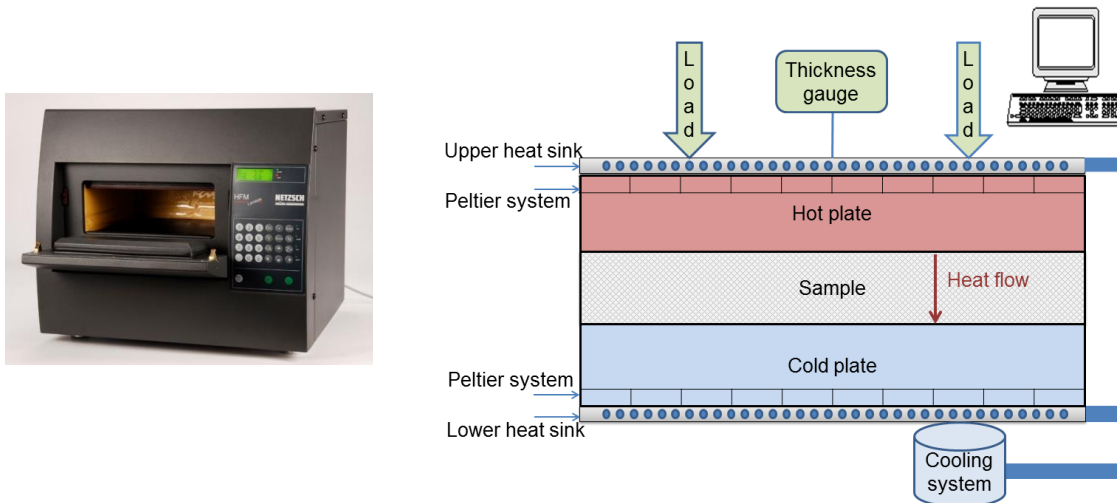
Figure 6. FTIR spectra of (a) CZ, and (b) TW aerogel blankets. ν shows stretching bond vibration, δ bond bending vibration and a asymmetric bond vibration.

2.3.1. Thermal Conductivity Measurements of the Dry Samples

The heat flow meter (HFM) method is based on establishing a steady-state, 1-D heat flux through a test specimen. In Figure 7, Netzsch HFM 436 Lambda, which is used for measuring the thermal conductivity of dry insulation samples (0.002 to $2 \text{ W}\cdot\text{m}^{-1}\cdot\text{K}^{-1}$) is shown. The instrument has been calibrated with a NIST-certified reference standard of known thermal conductivity. The

tests were conducted as per ASTM C518 standard. The sample, 30.5 cm×30.5 cm, with thicknesses ranging from 5 to 10 mm, were sandwiched between two metallic plates with a controlled temperature gradient, and mechanical load (pressure) control. The allowable range for implementing thermal conductivity tests using this device is -30 to 90°C (on the plates), therefore, in the present study, tests were performed with mean temperatures ranging from -20 to 80°C, temperature gradients of 20°C, and fixed pressure load of 0.5 Psi following ASTM C177. In HFM, sensors measure the heat flux and thermocouples measure the hot and cold plate temperatures. The HFM signal, Q (μV), is proportional to the heat flux \dot{q} across the sample, which is proportional to the temperature difference, ΔT , between the plates and inversely proportional to the total thermal resistance, R_{tot} :

$$\dot{q} = -k \frac{\Delta T}{\Delta x} = \frac{\Delta T}{R_{\text{tot}}} \quad (40)$$



(a) (b)
Figure 7. (a) The HFM instrument, and (b) its schematic.

2.3.2. Moisture Content Measurements

Moisture content prediction is a laborious task mainly due to the slow diffusion of moisture through porous materials, which makes the experimental study particularly long. In this study, water uptake of the aerogel blanket samples were measured following the ISO 12571:2013 Standard (Hygrothermal performance of building materials and products–Determination of hygroscopic sorption properties, Part B-climatic chamber method) [93]. Samples were placed in an environmental chamber, ESPEC Platinous series EPX-4H, capable of recreating a wide range

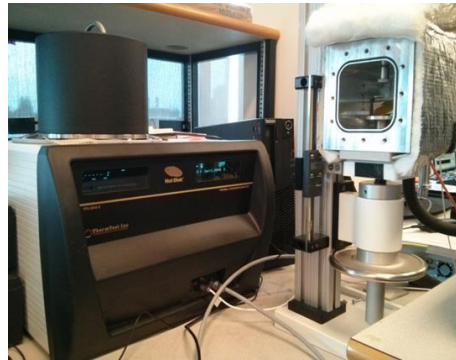
of temperature (10°C-85°C) and RH (0-98%) conditions. They were exposed to 0%, 40% and 90% RH at temperatures of 25°C and 45°C for 24 hours wetting process. Weights of the samples were measured after each wetting period, using Ohaus Adventurer™ Balance having 0.0001 g standard deviation. Prior to moisture sorption tests, the samples were dried, for 24 hours (according to our measurements the equilibrium was reached after 24 hours and the samples were completely dried), at 70°C under normal atmospheric pressure, and weighed to calculate the weight change after each wetting time. 70°C is safe, as the maximum possible temperature that the insulation materials can be used at is reported to be 125°C by the supplier[97],[98], and this temperature does not affect their physical and chemical structure.

2.3.3. Thermal conductivity Measurements of the Samples at Different Levels of RH

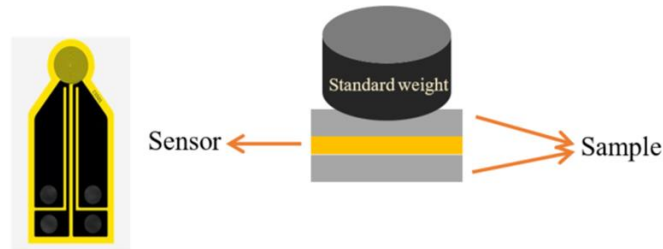
Thermal conductivity measurements at higher levels of RH were performed as per ISO22007-2 [99], using a transient plane source (TPS) thermal constants analyzer (TPS 2500S, ThermTest Inc., Fredericton, Canada). The temperature controlled chamber was modified to create an input and exit port for the flow of air with controlled humidity and a humidity sensor was added to the chamber. The flow of humid air was provided by a Cellkraft F-series humidifier. The humidifier operates through water transfer across a perfluorinated sulphonic acid membrane and is suitable for accurate humidity control without droplets. It can measure the gas temperature with $\pm 0.2^\circ\text{C}$ accuracy in the range of 0 to 50°C and $\pm 1.7\%$ for RH between 0 to 90%, i.e., the range used in this study. The temperature of the flowing humid air was matched to the temperature in the chamber. The flow rate was 6 nlpm (nominal litres per minute) with the RH under feedback control using the sensors within the chamber and the humidifier.

TPS device has several “hot disk” two-sided sensor types and software modules to conduct measurements on bulk materials (isotropic and anisotropic), thin films, powders and liquids. In this work, a sensor (TPS Hot Disk 7577) with a 2.001 mm radius nickel double spiral insulated in a thin layer of Kapton was used for simultaneous transient heating of the sample and precise temperature measurement. For bulk measurements, the sensor was placed between a pair of identical samples of 5 cm×5 cm×5 mm and compressed using a standard weight to minimize the thermal contact resistance. The sample-sensor assembly is shown in Figure 8. Each test was repeated three times to ensure the repeatability of the results. Low standard deviation of the measured data (about $2 \times 10^{-4} \text{ W}\cdot\text{m}^{-1}\cdot\text{K}^{-1}$) shows the reliability of the collected data. More

details of the methodology used in the thermal conductivity measurements can be found in Ref. [100].



(a)



(b)

Figure 8. Device (a) and simplified schematic of TPS (Transient Plane Source) thermal conductivity measurement (b).

2.4. Results and Discussion

The required input values for getting results from the developed model were parameters belonged to the samples of CZ and TW that either were measured by the author of the thesis (e.g. fiber and particle diameter, porosity and pore sizes, transmittance and thickness of the samples) or used from the manufacturers' data sheet (e.g. density and material of the fibers). The governed equations were solved for a cubic unit cell having $40\mu\text{m}$ dimensions for CZ and $20\mu\text{m}$ for TW, using MATLAB, to predict the effective thermal conductivity of the mentioned aerogel blankets. In the following section, a comparison of modeling results and the experimental data is provided, followed by parametric studies in which the effects of variable parameters on the effective thermal conductivity of aerogel blanket are examined.

2.4.1. Model Validation and Parametric Studies for the Dry Samples

The test conditions mentioned in section 2.3.1 were applied to the samples of aerogel blanket. It was detected that aerogel blanket samples spread fine particles of silica dust during the measurement of k-value using HFM. Four original dry aerogel blanket samples were placed in and removed from the HFM multiple times and the thermal conductivities of these samples were measured for each placement/removal. The results specified that the handling does not contribute in changing the k-value. Consequently, each sample is tested for three times with the same temperature conditions; the standard deviations are less than $10^{-3} \text{W}\cdot\text{m}^{-1}\cdot\text{°C}^{-1}$.

Presented in Figure 9, good agreement was observed between the experimental and modeling results of the effective thermal conductivity variation of dry CZ and TW over a temperature range of -20 to 80°C. The highlights of Figure 9 are:

- Higher temperature leads to higher thermal conductivity;
- By increasing the temperature from -20 to 80°C, the effective thermal conductivity increases approximately 12% for CZ and 30% for TW, which is due to higher radiation and gas conduction heat transfers for TW compared to CZ; and
- The effective thermal conductivity of CZ is less than TW, which was consistent with manufacturer data sheet. It can be because of lower thermal conductivity of fibers and smaller blanket pore sizes in this composite.

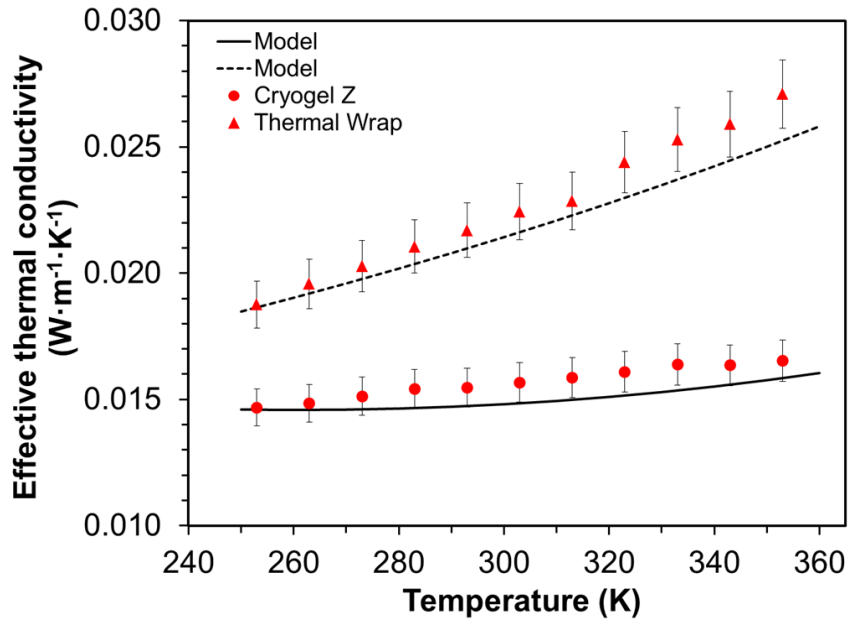
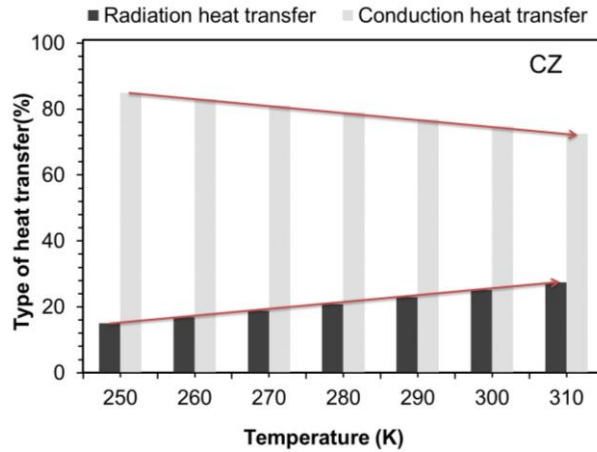
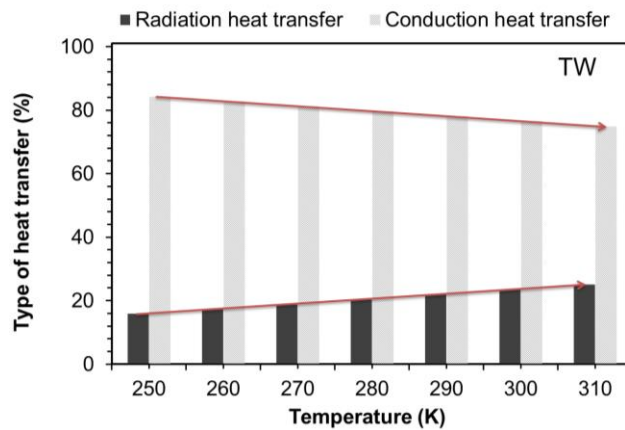


Figure 9. Temperature dependence of the thermal conductivity of dry CZ and TW aerogel blankets.

Figure 10 shows a comparison of the contribution of each heat transfer mode (percentage of the total heat transfer) in the total heat transfer in CZ and TW. It reveals that the major portion (about 95%) of the heat transfer is due to the conduction (gas and solid). It should be noted that this contribution decreases with increasing temperature because the radiation contribution rises and this effect is more prominent in TW samples.



(a)



(b)

Figure 10. Contribution of each type of heat transfer (%) on total heat transfer rate; (a) CZ, and (b) TW.

The developed model can be conveniently used to systematically study the effect of aerogel blanket microstructural parameters, thermophysical properties, and operating conditions on its effective thermal conductivity. The important parameters that produce noticeable variations in the effective thermal conductivity are fiber thermal conductivity and porosity of the blanket. The objective is to investigate optimized values for such parameters, which can lead to new designs of aerogel composites with lower effective thermal conductivity. As shown in Figure 11, fibers thermal conductivity, as one of the influential factors in the aerogel blanket structure, has a minor effect on the effective thermal conductivity of the blanket, keeping the other parameters constant. This analysis provides more appropriate options for choosing low thermally conductive fibers along with the cost and availability.

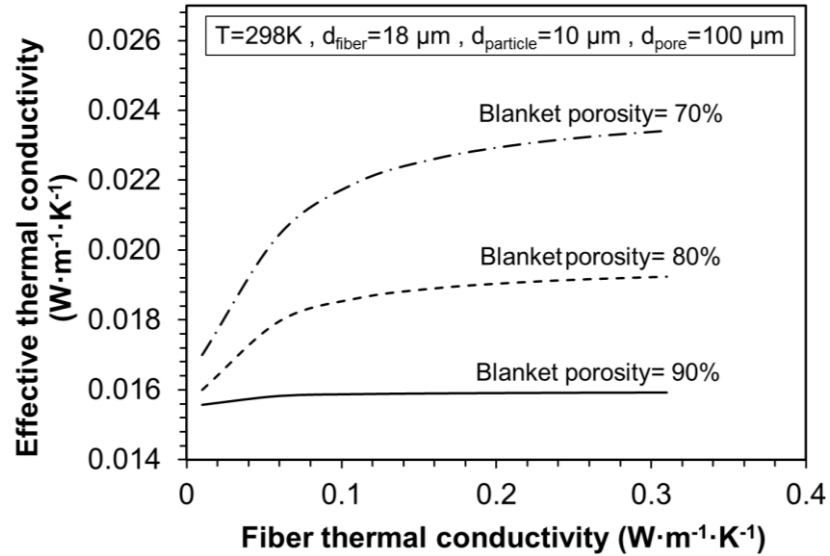


Figure 11. Effect of fiber material thermal conductivity on the effective thermal conductivity

Figure 11 highlights are:

- The lower the blanket porosity, the higher the effective thermal conductivity; and
- By decreasing the blanket porosity from 90% to 70%, the thermal conductivity increases about 40%, which is prominent.

It should be noticed that high blanket porosity can be interpreted as a few large pores or lots of small pores. Large pore size results in higher porosity which might be a factor for having less effective thermal conductivity. On the other hand, larger pore sizes create larger gaps which lead to having convection heat transfer, more conduction through gas molecules and more effective thermal conductivity. This issue is addressed in aerogel blanket by creating large surface areas in combination with nano-porous pathways. Hence, high porosity and small pore sizes are keys to low thermal conductivity in aerogel blankets.

Low thermal conductivity in aerogel blankets is due to its nature as a highly porous solid material, which means almost no gas convection, very small gas and solid conduction, and small radiation heat pathways. Hence, as it can be understood from Figure 12, reducing the porosity eliminates the leverage of using aerogel blankets as an insulation material and in this case, using the other conventional types of insulations may be more prudent.

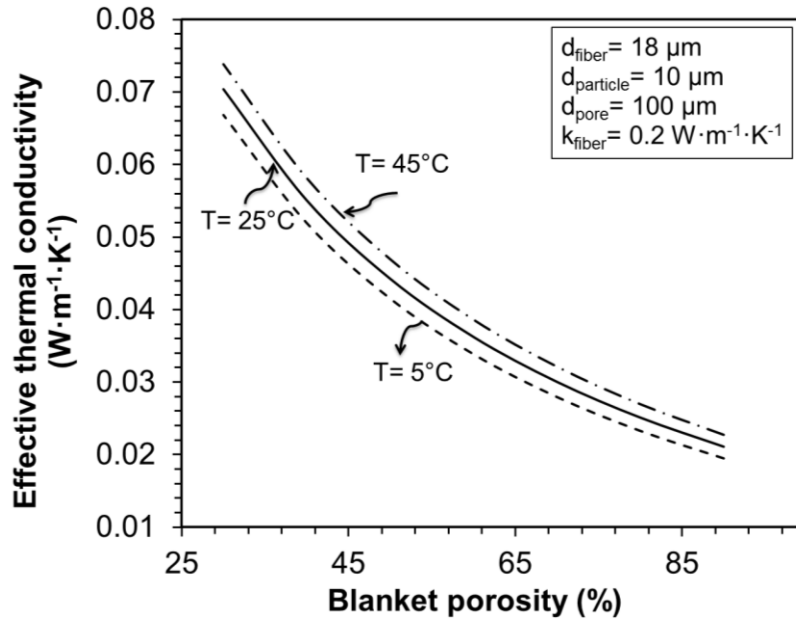


Figure 12. Effect of blanket porosity on the effective thermal conductivity.

The effect of alpha which is the deformed factor to show the area contact between the spheres instead of point contact on the effective thermal conductivity of aerogel blankets is shown in Figure 13. The results showed that by increasing alpha from 0.1 to 1, 5% increase in k_{eff} can be observed which is negligible.

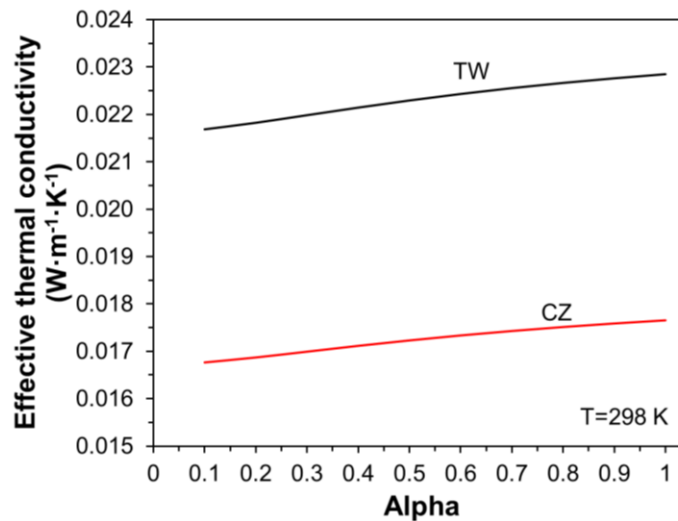


Figure 13. Effect of deformed factor on the effective thermal conductivity.

Additionally, the effect of temperature history on thermal conductivity of the available samples was investigated. A fixed, periodic temperature of -20 and 80°C, was applied on each

sample for 10 cycles. As it is shown in Figure 14 and Figure 15, k-value variation was stable during all the cycles and peak to peak thermal conductivity values stayed constant. Therefore, it can be concluded that 100°C temperature variation affects the k-value, however, accelerated temperature variation from -20 to 80°C does not have any hysteresis effect on thermal performance of aerogel blanket samples.

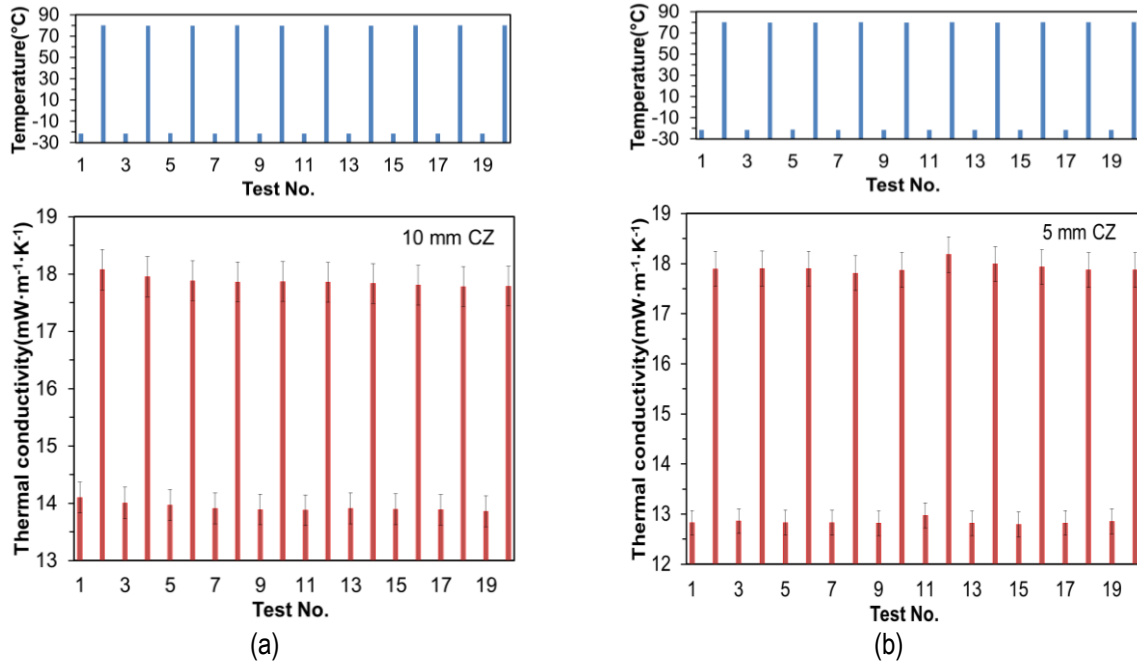


Figure 14. Thermal conductivity variation during temperature cycling for CZ, (a) 10 mm, and (b) 5 mm thickness.

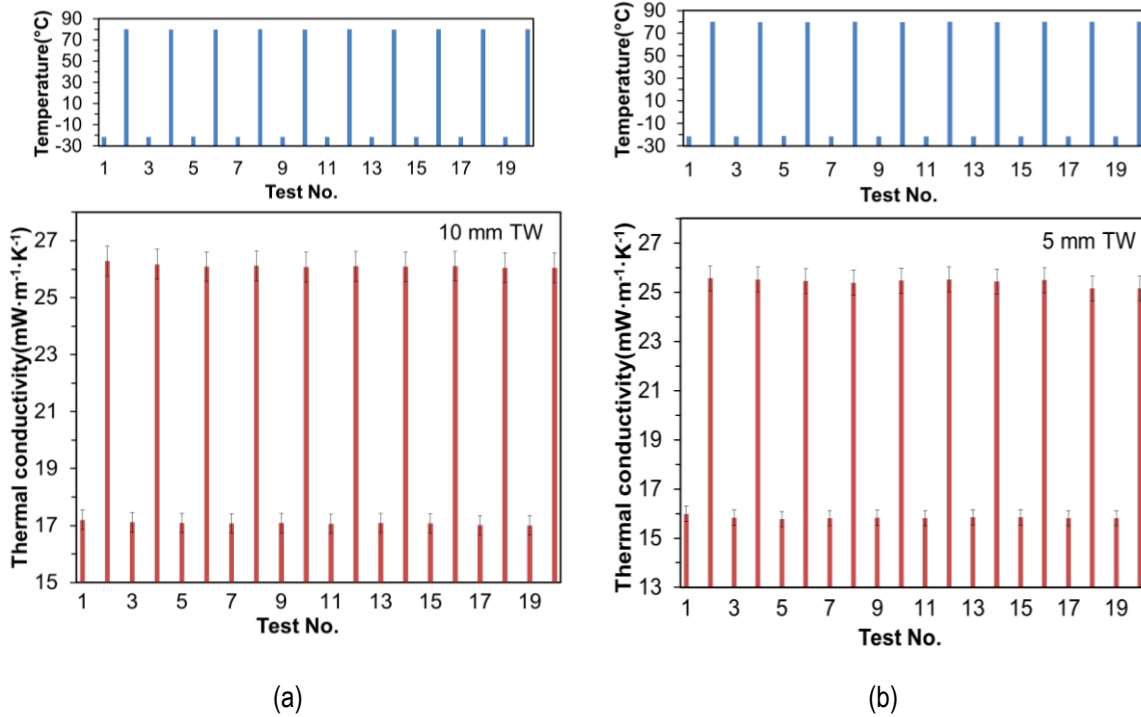


Figure 15. Thermal conductivity variation during temperature cycling for TW, (a) 8 mm, and (b) 5 mm thickness.

2.4.2. Model Validation and Parametric Studies for the Samples at Different Levels of RH

Sorption isotherm measurements

Sorption isotherms (the moisture taken up from the air as a function of RH), is one of the important characteristics of materials. Due to the complexity of sorption processes, isotherms cannot be calculated theoretically and should be measured experimentally for each material [46]. Figure 16 shows the sorption isotherms for the samples of aerogel blanket at two different temperatures to see the effect of temperature on moisture content as well. The error bars show the standard deviation of the measurements. The plots demonstrate that increasing humidity and decreasing temperature increase the moisture content since at higher temperatures, the transport of water molecules is faster, the bonds can be released more easily, and therefore the amount of adsorbed water decreases. Furthermore, the maximum amount of moisture uptake is 2.87% of dry mass for TW and 2.34% of dry mass for CZ measured at 25°C. The slight difference between CZ and TW water uptakes is likely due to different pore size distributions of the two materials. Figure 17 clearly shows that the observed weight increase in the samples after wetting for 34 hours is due to liquid water formation inside the pores (adsorbed water), i.e., if all the pores were

filled with water vapor (at a given RH and T), the weight increase of the samples would be order of magnitudes less than the measured values. Therefore, weight of the water vapor has been neglected in the modeling section, compared to the adsorbed water, and the defined moisture content (m_w) just shows the weight of the water content.

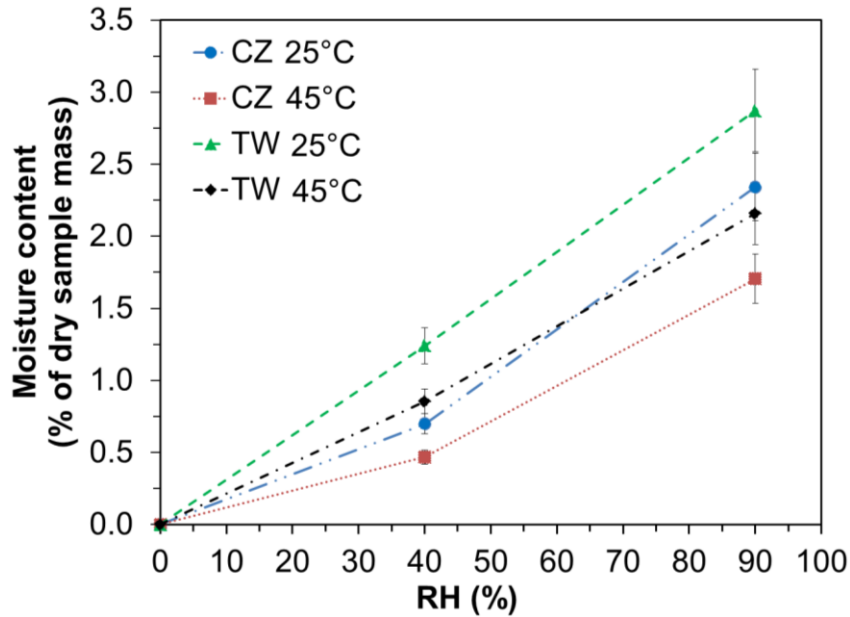


Figure 16. Sorption isotherms at 25°C and 45°C for CZ and TW aerogel blanket samples.

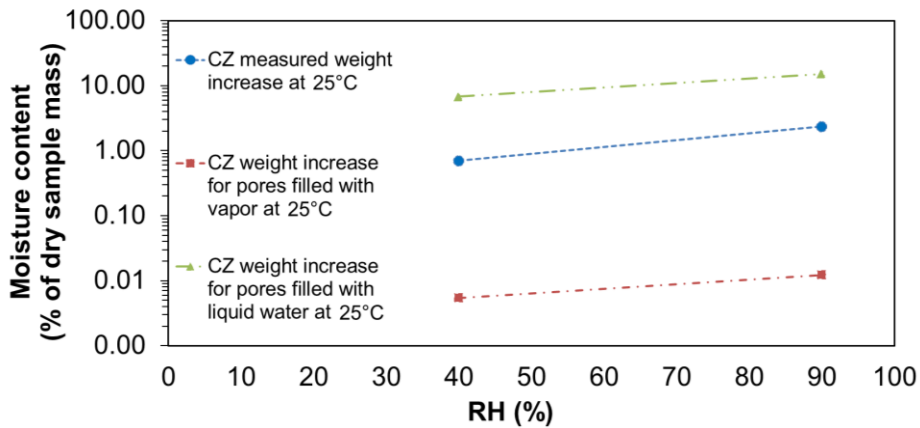


Figure 17. CZ weight increase in three cases: blue line: actual measured data; red line: water vapor filled the pores; and green line: adsorbed water.

Thermal conductivity analysis at the transient regime

For each aerogel blanket type, two 5 mm thick pairs of 5 cm×5 cm square samples were prepared to be tested at different levels of RH and temperature using our TPS-humidifier

assembly. Cyclic thermal conductivity measurements of aerogel blankets were performed between 0% and 80% RH, with power of 10 mW and measurement time of 40 s in short intervals. In Figure 18, each data point was measured after 5 hours rest time, after changing the humidity condition. The measured data revealed that thermal conductivity was increased over time, at cycles with the same RH. This can be interpreted as a result of moisture accumulation inside the pores. It also shows that it should take more than 5 hours for the moisture to leave the pores. Besides, it is observed that after approximately six cycles, the effective thermal conductivity reaches its maximum, which means the material was holding all the humidity that it could.

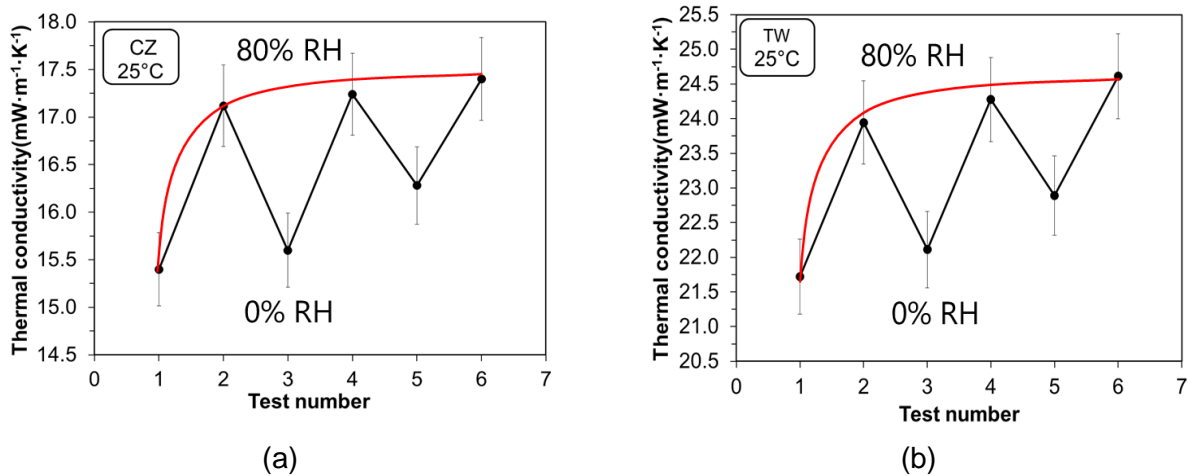


Figure 18. Cyclic thermal conductivity measurements of CZ and TW between 0% and 80% RH at 25°C.

To find the diffusion coefficient (D) defined in Eq.(18), a series of long-term experiments on CZ were performed using TPS-humidifier assembly. The dry sample of CZ was placed inside TPS at 25°C, under fixed conditions of 20%, 40% and 80% RH for more than a month and the thermal conductivity was measured at different time intervals from 5 hours to weeks to ensure that steady-state was reached. Before each set of measurements, the dry sample was tested at 0% RH, in different time intervals to ensure that its thermal conductivity remains constant over time.

An optimization method (Genetic algorithm with the parameters of: population size of 50, generations and selection rate of 100%, migration rate of 10% and mutation rate of 90%) [101] was applied on the data set of 80% RH, to obtain the appropriate diffusion coefficient (D) of CZ. The objective function is shown in Eq.(41):

$$\min \text{ error} = \sum (k_{\text{eff_humid_model}}(t) - k_{\text{eff_humid_data}}(t))^2 \quad (41)$$

The fitted value of D was used for modeling the moisture content of CZ at any other RH condition following Eq.(22). Since the model accurately predicts the data set of 20% and 40% RH, as shown in Figure 19, the fitted value of D is reliable. A sensitivity analysis on the typical values of D is presented in Figure 20 for three times after changing the RH to 20%, i.e., 1 hour, 10 hours, and 25 hours. It shows that changing D in the range of 10^{-10} to $10^{-6} \text{ m}^2 \cdot \text{s}^{-1}$ changes the effective thermal conductivity less than 2%. It also demonstrates that at the beginning of the diffusion process ($t=1 \text{ hr}$), the diffusion coefficient has a stronger effect on the effective k -value compared to the steady-state condition.

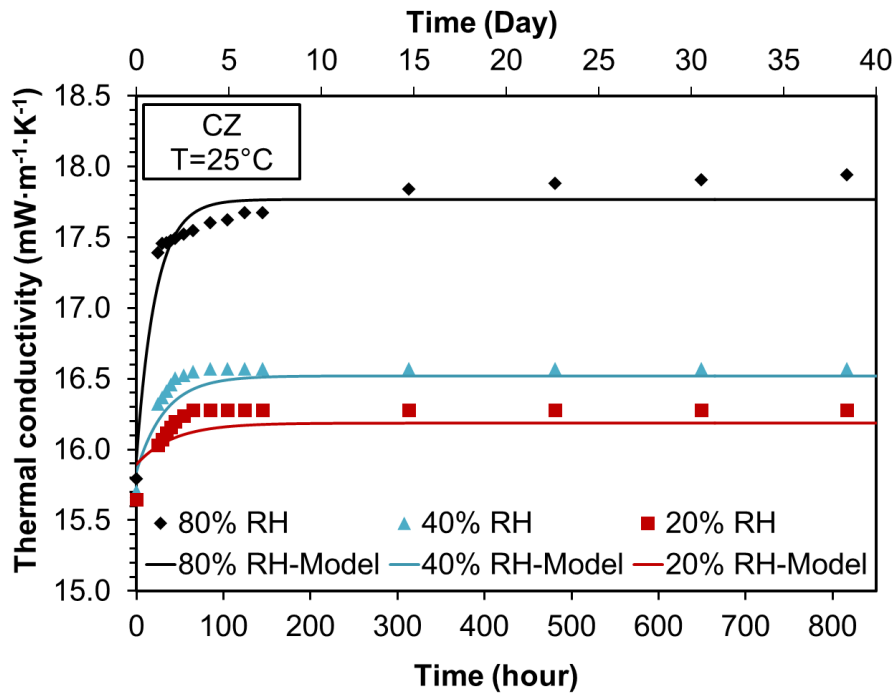


Figure 19. Thermal conductivity of CZ over time at 25°C and 20%, 40% and 80% RH.

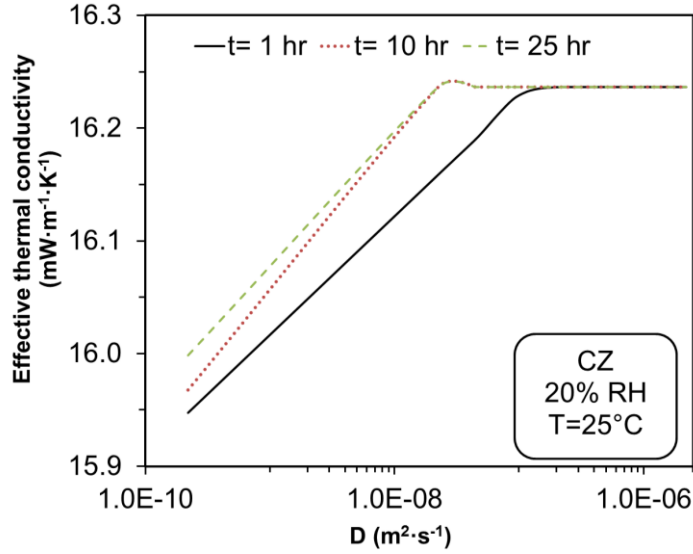


Figure 20. Sensitivity analysis on CZ diffusion coefficient at 20% RH and 25°C.

Figure 19 shows that it took about 20 hours for thermal conductivity of CZ at 80% RH to reach steady-state condition, which is due to the diffusion resistance and storage capacitance of the sample. Water volume fraction increase (percentage of the pore volume) is also shown over time in Figure 21, which indicates that in a humid environment, moisture gradually replaces air in the pores until no concentration gradient throughout the sample exists.

Values of diffusion coefficient (D) and time constant (τ) are shown in Table 2-3. As it is shown in this table, it takes more time for CZ to reach to steady-state condition at higher RH, because of the higher vapor partial pressure gradient between the dry aerogel and ambient at higher RH.

Table 2-3. Diffusion parameters of CZ at different RH.

	20% RH	40% RH	80% RH
$D(m^2 \cdot s^{-1})$	2.2×10^{-9}		
τ (hours)	12.37	14.00	19.59

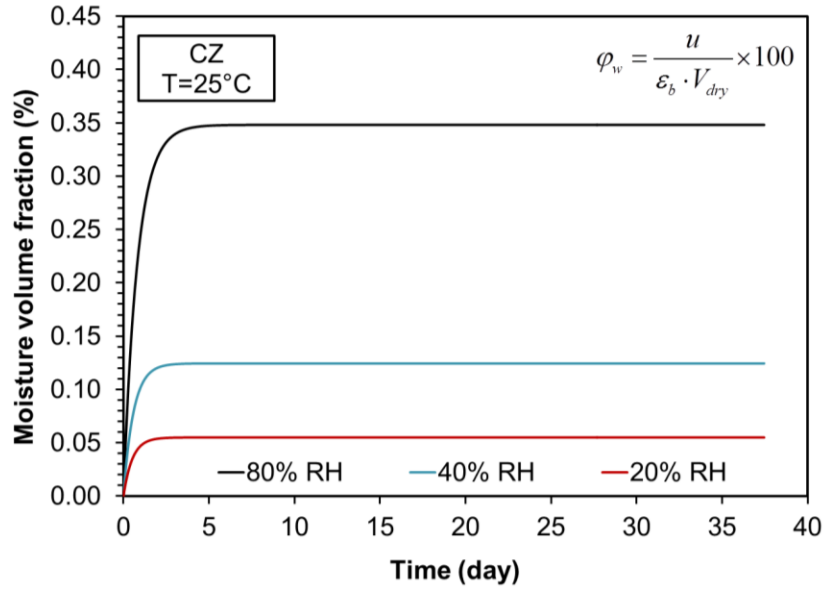


Figure 21. Moisture volume fraction of CZ over time at 25°C.

Thermal conductivity analysis at the steady-state regime

The thermal conductivity of each pair of samples was measured in TPS-humidifier assembly with a power of 10 mW, measurement time of 40 s and the rest interval of 24 hours between measurements to ensure steady-state condition is reached. Figure 22 and Figure 23 present the effective thermal conductivity of aerogel blanket samples as a function of RH at two temperatures of 25°C and 45°C.

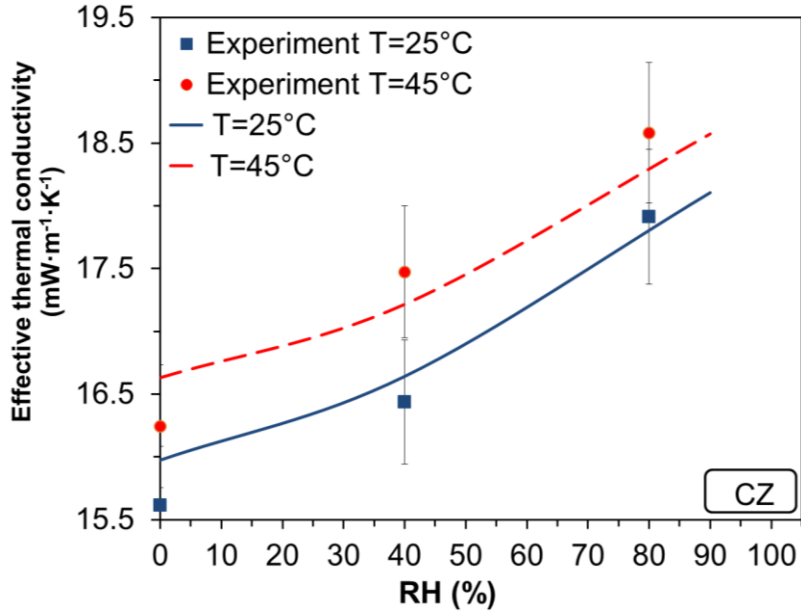


Figure 22. Effective thermal conductivity as a function of RH for CZ at 25°C and 45°C.

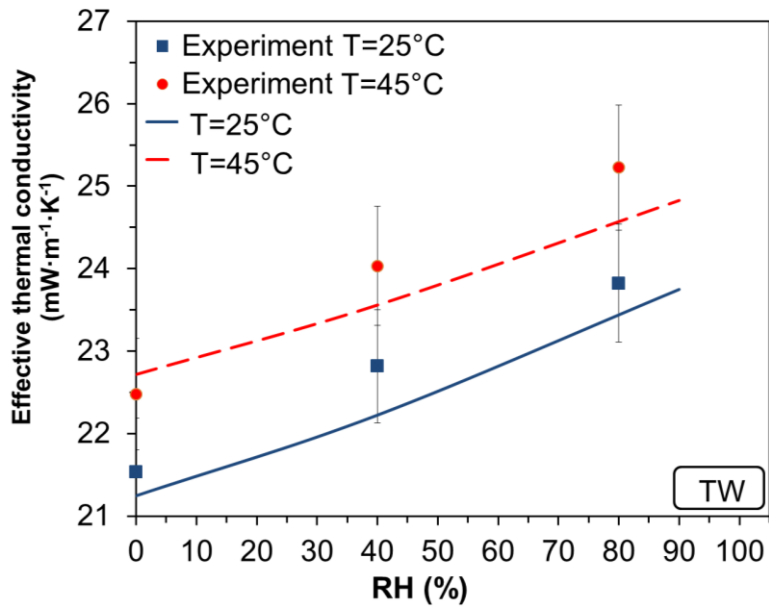


Figure 23. Effective thermal conductivity as a function of RH for TW at 25°C and 45°C.

Results show that increasing the RH from 0% to 90% increases the k-value ~14% for CZ and ~11% for TW after reaching steady-state. This thermal conductivity increase is a result of water accumulation inside the pores at higher RH that replaces the dry air and results in higher heat transfer rate inside the material. Also, according to Figure 22 and Figure 23, the modelling results at 25°C and 45°C (the solid and dash lines) become closer at higher RH. The reason is

that having more moisture content at the lower temperature (See Figure 16) leads to a slightly sharper thermal conductivity increase at 25°C.

According to Eq.(33), Z constant of CZ and TW at 25°C can be calculated from Figure 24. The slope of the curve shows $k_{eff_dry} \times Z$ and the intercept represent k_{eff_dry} . Therefore, moisture supplement of the thermal conductivity of CZ and TW are 6.72 and 3.81, respectively. The higher the moisture supplement, the stronger effect on the effective thermal conductivity at humid condition.

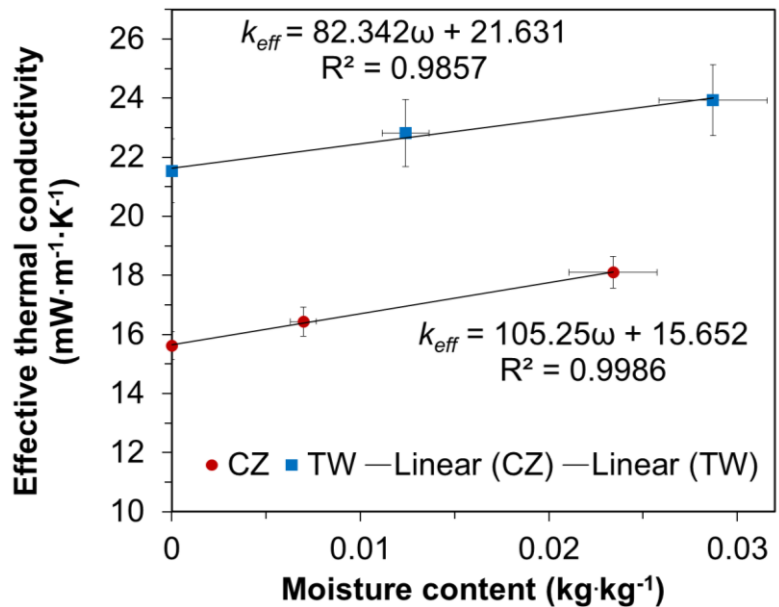


Figure 24. The change in the thermal conductivity as a function of moisture content at 25°C

Chapter 3.

Mechanical Deformation Analysis of Aerogel Blankets

Silica aerogel tends to crack after repeated usage, which affects the long-term performance of the aerogel blanket insulation materials, in terms of porosity, thickness, and thermal resistance. Therefore, the mechanical behavior of aerogel blankets under compression should be understood. In this research, the mechanical performance of two types of aerogel blanket samples under compression and after repeated cycling load is studied. Additionally, the proposed unit cell approach in the previous chapter is modified to develop a mechanistic analytical model for predicting the compressive stress-strain relationship of aerogel blankets. In this model, only aerogel blankets microstructural properties, such as fiber and particle diameters, elastic modulus, and porosity are used. Bending of fibers is considered as the main deformation mechanism at the unit cell level and overall blanket deformation is calculated from the summation of the deformations of all the unit cells. Employing the proposed model, the stress-strain relationship is presented and verified using the experimental data. The results of this chapter are published in the Energy and Buildings journal [102]. The experimental studies were all performed by the author of the thesis. In defining the geometry of the problem and developing the analytical model the co-authors have had major contributions.

3.1. The Present Model

SEM images of the aerogel blankets revealed a repetitive microstructural arrangement of fibers and aerogel particles leading to a unit cell approach for the analytical model. Figure 25 (a) shows a SEM image of a CZ aerogel blanket. Figure 25 (b) represent the geometry of the proposed unit cell, which is a modified version of the unit cell in section 2.1.4. And Figure 25 (c) displays the solution domain, which is obtained after identifying the symmetry lines of the unit cell. By mirroring the solution domain across each plane (x , y and z), the unit cell can be produced. This unit cell, designed to model the mechanical behavior of aerogel blanket under compression, includes fibers surrounded by small aerogel particles with a large particle at the center. Each fiber is modeled as a bending beam supported through a contact point with the fiber below. Force is applied to each fiber through a contact point with a fiber above that is one edge of the unit cell, l_{fiber} , away from the supporting contact point.

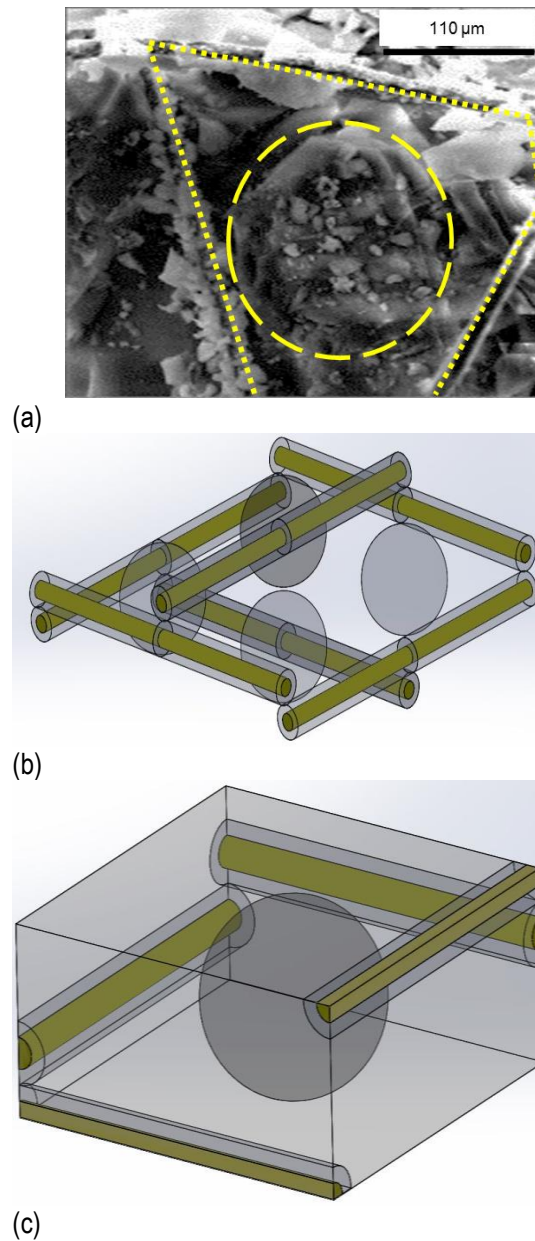


Figure 25. (a) SEM image of aerogel blanket (CZ) showing aerogel coated fibers (marked with dotted lines) and aerogel filled pores, and (b) Geometry of the proposed unit cell, and (c) schematic of the solution domain showing fibers coated with a layer of aerogel particles, a larger spherical aerogel particle at the center, a force, F' , applied to the uppermost fiber and the fibers length in the unit cell, l_{fiber} .

In our approach, two different porosities were considered: 1) porosity of the aerogel coating on the fibers, which is about 96% for aerogel particles, ϵ_a ; and 2) porosity of the blanket, ϵ_b . The assumptions used in the model development are listed below:

1. Smooth sphere and fiber surfaces, *i.e.*, no rough contacts on sphere-sphere and fiber-sphere contact points;
2. No contact point between the large particle at the center and the fiber-aerogel composite, *i.e.*, the solution domain aspect ratio is $l_{fiber}/D_p \geq 2$. For this assumption to be applicable, the range of the applied load should be limited to less than 10 kPa, that is in the range of the load applied on such material in our experiments due to equipment limitations; and
3. Negligible deformation for aerogel particles (Hertzian contact), compared to bending fibers deformation ($\delta_{max_fibers} \sim 10^{10} \delta_{max_particles}$).

The length of the fibers in each solution domain, l_f (m), is equivalent to the length of the two edges of the solution domain, and can be found from the porosities using the following equation:

$$1 - \varepsilon_b = \frac{V_{solid}}{V_{tot}} = \frac{\frac{3\pi}{8} D_{fiber}^2 l_f + \frac{3\pi}{2} l_{fiber} (D_{fiber} t_a + t_a^2) (1 - \varepsilon_a) + \frac{4\pi}{3} \left[3 \left(\frac{D_{fiber}}{2} + t_a \right) \right]^3 (1 - \varepsilon_a)}{6 l_{fiber}^2 \left(\frac{D_{fiber}}{2} + t_a \right)} \quad (42)$$

where V_{solid} is the solid volume of the domain, V_{tot} is the total volume of the domain, D_f is the diameter of the fibers, and t_a is the thickness of the layer of aerogel on the fibers, which is assumed to be equal to an aerogel particle diameter. The third edge of the solution domain can be calculated from the fibers and aerogel layer thickness ($3 \times (D_{fiber} + 2t_a)$). From the length of the fibers and the compressive force, which is assumed to be applied on the end point of the fiber on top, the deflection of the domain in the z direction can be calculated according to the beam theory for beams supported on both ends and single load at the center, Figure 26(a) [103]. Also, according to the second and third modeling assumptions, the large spherical aerogel particles are only contributing to the effective porosity of the solution domain and do not affect the total deformation, so the stress-strain analysis is applied on the simplified solution domain, as shown in Figure 26(b).

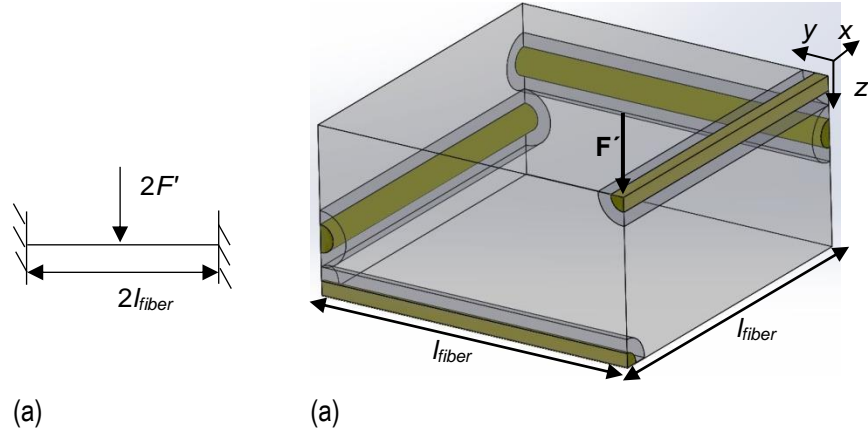


Figure 26. (a) Schematic of the applied beam theory, and (b) the solution domain used in stress-strain analysis.

The unit cell deflection is calculated from Eq.(43):

$$\delta_u = 4 \times \delta_{Beam} \quad (43)$$

where the deflection of each beam, δ_{Beam} (m), is

$$\delta_{Beam} = \frac{F' \times l_{fiber}^3}{3(EI)_{eff}} \quad (44)$$

and the applied force on one solution domain (N) is:

$$F' = \frac{F_{tot}}{N_u} \quad (45)$$

and N_u is the number of solution domains in one layer, obtained using the Eq. (46):

$$N_u = \frac{A_{sample}}{l_{fiber}^2} \quad (46)$$

in which A_{sample} is area of the sample (m^2). $(EI)_{eff}$ ($Pa \cdot m^4$) is the effective flexural rigidity of the beam, which can be calculated using elastic modulus of fibers and aerogel particles, E (Pa), and their second moment of inertia, I (m^4), according to Eq.(47):

$$(EI)_{eff} = (EI)_{fiber} + (EI)_{aerogel} \quad (47)$$

where $I_{fiber} = \frac{\pi}{2} (D_{fiber} / 2)^4$ and $I_{aerogel} = \frac{\pi}{2} \left((D_{fiber} / 2 + t_a)^4 - (D_f / 2)^4 \right)$. However, the EI term corresponding to aerogel layer is negligible compared to fibers elasticity, thus, is not considered in the model.

To calculate the total deformation of an aerogel blanket, the number of layers should be multiplied by the deformation of one layer, which equals the deformation of one solution domain ($\delta_{layer} = \delta_u$). The number of layers in the through-plane direction can be calculated from:

$$N_{layers} = \frac{t_b}{6 \left(\frac{D_{fiber}}{2} + t_a \right)} \quad (48)$$

where t_b is the thickness of the aerogel blanket. Since the deformation of one layer equals the deformation of one domain, finally, the total deformation can be reported as:

$$\delta_{tot} = N_{layers} \times \delta_{layer} \quad (49)$$

Therefore, by combining Eq. (43) to Eq.(49), the total deformation of an aerogel blanket under a compressive mechanical pressure (P_{tot}) can be obtained from a closed form analytical relationship shown in Eq.(50):

$$\delta_{tot} = \frac{4t_b P_{tot} l_f^5}{9(D_f + 2t_a)(EI)_{fiber}} \quad (50)$$

Eq. (51) is a compact relationship between the compressive strain, e , and the compressive mechanical pressure or stress, presented as follows:

$$e = P_{tot} \left(\frac{4l_{fiber}^5}{9(D_{fiber} + 2t_a)(EI)_{fiber}} \right) \quad (51)$$

Compressing aerogel blankets results in a change in its microstructure, thus the porosity varies with compression. Assuming that the volume of fibers and aerogel particles (solid volume) do not change at each loading step and only the pore volume decreases, the new porosity can be calculated using the new thickness of the sample. Therefore, the expected porosity can be defined based on the relation for a change in volume, where M is the compression factor (ratio of

the uncompressed blanket thickness to the compressed thickness at each loading step; i.e., $t_{b,initial}/t_{b,new}$ where $t_{b,initial}$ and $t_{b,new}$ are the initial and new thickness of the aerogel blanket, respectively, and ε_b is the void fraction of the aerogel blanket material ($0 < \varepsilon_b < 1$).

$$\varepsilon_{b,new} = 1 - M(1 - \varepsilon_{b,initial}) \quad (52)$$

Using Eq.(52), the new porosity can be obtained after each load increment and thickness calculation. The algorithm for this porosity modification is presented in Figure 27.

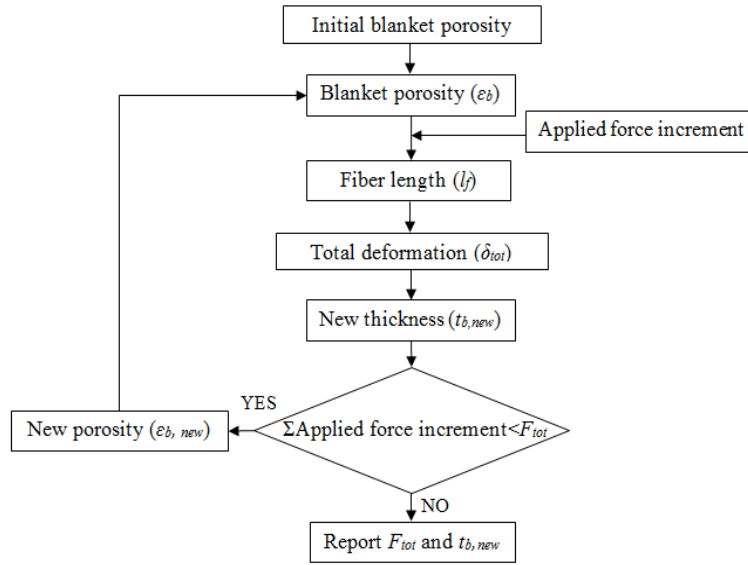


Figure 27. Porosity modification algorithm.

The mentioned algorithm can be expressed in an analytical relationship as follows to calculate the blanket deformation directly at each loading step, Eq.(53):

$$\lim_{n \rightarrow \infty} \delta_i = t_{b,i-1} \frac{P_{tot,i}}{n} \frac{2l_{fiber,i-1}^5}{9(EI)_{fiber} \left(\frac{D_{fiber}}{2} + t_a \right)}, \quad i = 1, \dots, n \quad (53)$$

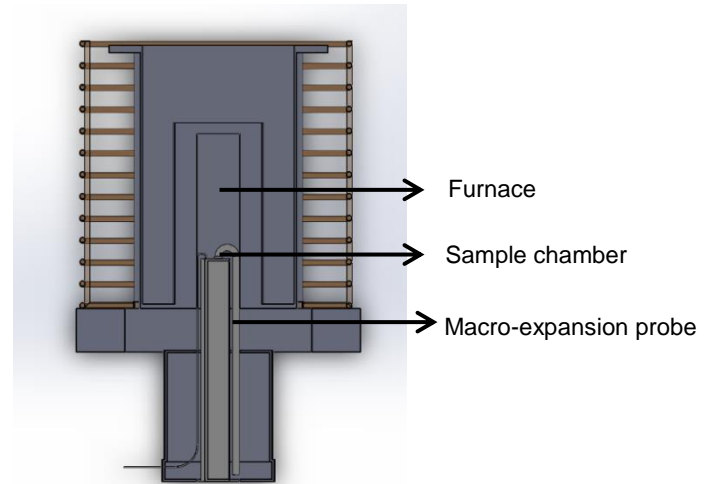
where $l_{fiber,i-1}$ has to be calculated from Eq.(54):

$$l_{fiber,i-1} = \frac{\pi D_{fiber}^2 + 4\pi(1-\varepsilon_a)(D_{fiber}t_a + t_a^2) + \sqrt{16\pi} \sqrt{3072(1-\varepsilon_a)\left[\frac{t_{b,initial}}{t_{b,i-1}}(1-\varepsilon_{b,initial})\right]\left(\frac{D_{fiber}}{2} + t_a\right)^4 + \pi\left(\frac{1}{4}D_{fiber}^2 + (1-\varepsilon_a)(D_{fiber}t_a + t_a^2)\right)^2}}{32\left(\frac{D_{fiber}}{2} + t_a\right)\left[\frac{t_{b,initial}}{t_{b,i-1}}(1-\varepsilon_{b,initial})\right]} \quad (54)$$

3.2. Experimental Study

In this study, the same samples mentioned in Table 2-2 are used to perform compression tests and cycling study using HFM and TMA. Another feature of HFM is regulating the compression precisely and measuring the sample thickness with controlled loads up to 21 kPa.

A TMA (Q400EM, TA Instruments) with a macro-expansion probe with a 6.07 mm diameter contact area was used to compress 7 mm×7 mm insulation samples. Two samples of each of type of the aerogel blanket insulations were tested with a linear ramp force up to 0.4 N in a dry nitrogen environment at room temperature. A schematic of the TMA instrument is shown in Figure 28. TMA measures sample displacement at various temperatures, times, and applied forces and its resolution for displacement is less than 0.5 nm.



(a) (b)
Figure 28. (a) TMA device, and (b) its schematic [104]

The changes in the morphology of the material after compression were evaluated by Nano-SEM. For this purpose, samples were pressed up to a predetermined load at room temperature (ex-situ), which was the maximum load applied on the samples using HFM and TMA (8 kPa), and the images were taken under no-load and compressed conditions. In these images,

Figure 29, the compressed material does not show any noticeable difference compared to its original state, comparing the solid parts.

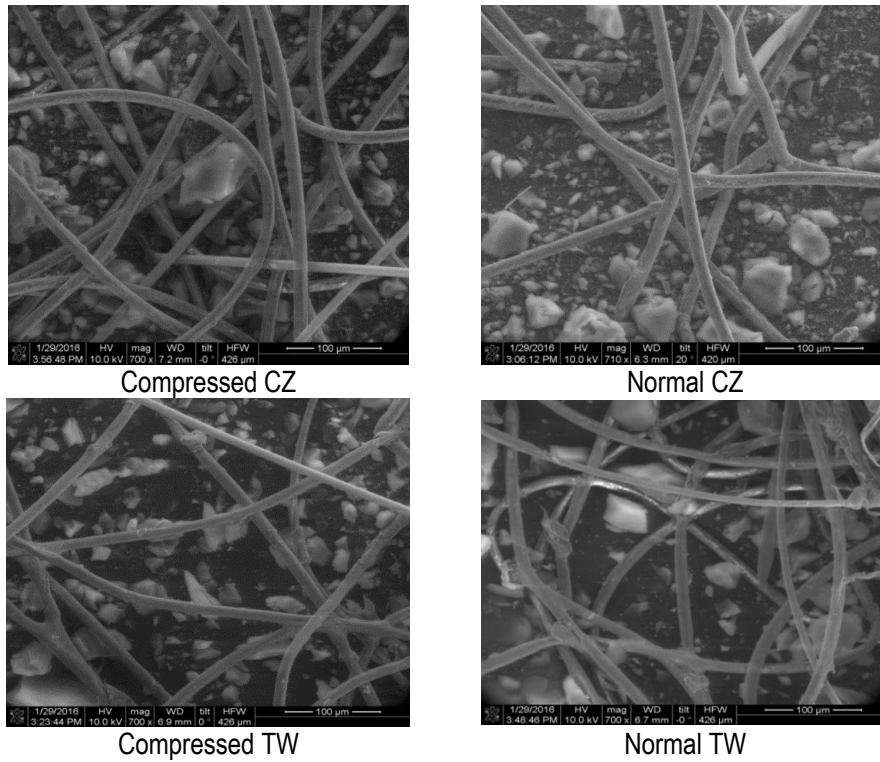


Figure 29. Microstructure of aerogel blanket samples; at no-load and compressed conditions. The scale bars show 100 µm.

3.3. Results and Discussion

In section 3.1, a nonlinear model is developed to predict the deformation of aerogel blanket samples as a function of the stress applied on them. The parameters used in the analytical model are presented in Table 3-1 and the model was solved for a 200 µm long unit cell for CZ and 100 µm long unit cells for TW. The unit cell used for modeling the deformation of aerogel blankets is an extension of the unit cell used for modeling the effective thermal conductivity and represents a larger portion of the material structure.

Table 3-1. Constant parameters used in the compression analytical model.

Sample	Thickness	Fiber modulus of elasticity	Particle modulus of elasticity [105]
CZ	10±0.5 mm	85 Gpa [106]	3 Mpa
	5±0.5 mm		
TW	8±0.5 mm	3.5 Gpa [107]	3 Mpa
	5±0.5 mm		

Figure 30 to Figure 33 present the results of the experiments performed by HFM and TMA and comparison to the developed model. The results of the proposed approach agreed well with the experimental data with low relative difference (maximum 15%) and show that compression had minimal effect on the aerogel blanket insulation materials compared to the conventional insulation materials, e.g., cellulose, rock wool, and fiberglass. In Ref. [51], large strain was measured under relatively low load. The authors reported 40% strain in fiberglass, 26% strain in rock wool, and 20% strain in cellulosic insulation material, after applying a maximum of 0.14 kPa on the samples with initial thickness of 30 cm.

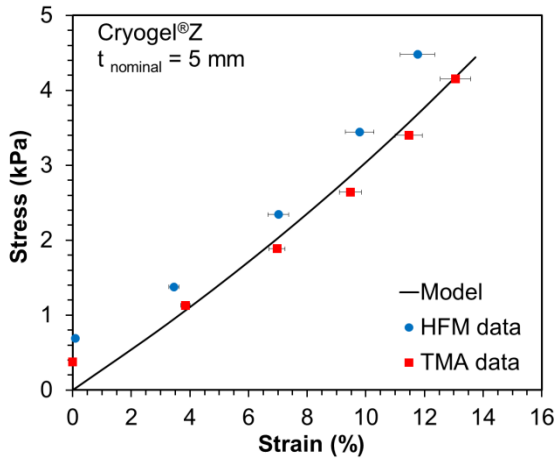


Figure 30. Stress-strain data and modeling result for CZ with 5 mm nominal thickness.

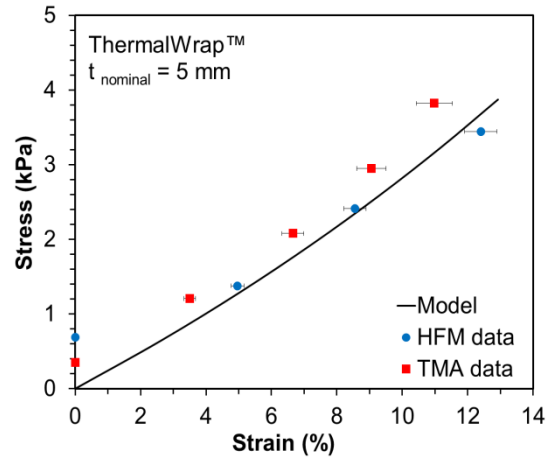


Figure 31. Stress-strain data and modeling result for TW with 5 mm nominal thickness.

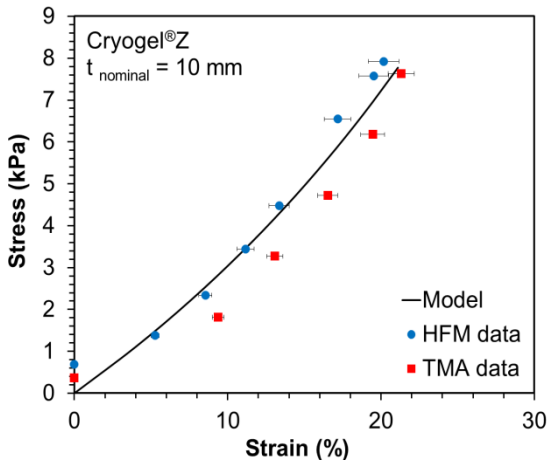


Figure 32. Stress-strain data and modeling result for CZ with 10 mm nominal thickness.

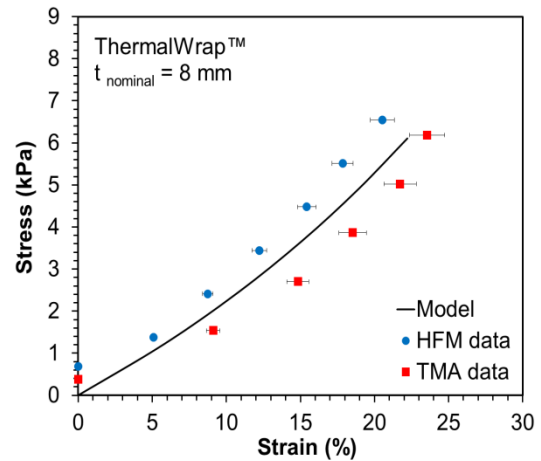


Figure 33. Stress-strain data and modeling result for TW with 8 mm nominal thickness.

The important parameters affecting the results of the analytical model for predicting the strain of aerogel blankets are fiber and particle sizes. A sensitivity analysis is performed on the effect of these parameters to study the model limitations and practicality. As shown in Figure 34, smaller aerogel particle size is the main reason for having small strain in aerogel blankets, which is due to the fragile structure of aerogels. In other words, large particle size adds to the brittleness of aerogel blankets structure and leads to having very large strain under heavy mechanical loads. Larger fiber diameter results in mechanically stronger structures for aerogel blankets under uniaxial compression, as shown in Figure 35. However, in the model there is a limitation for the

aspect ratio ($l_{fiber}/D_p \geq 2$), such that there is no contact between the large particle at the center and the aerogel coated fibers, which constrains obtaining the minimum possible strain for aerogel blankets.

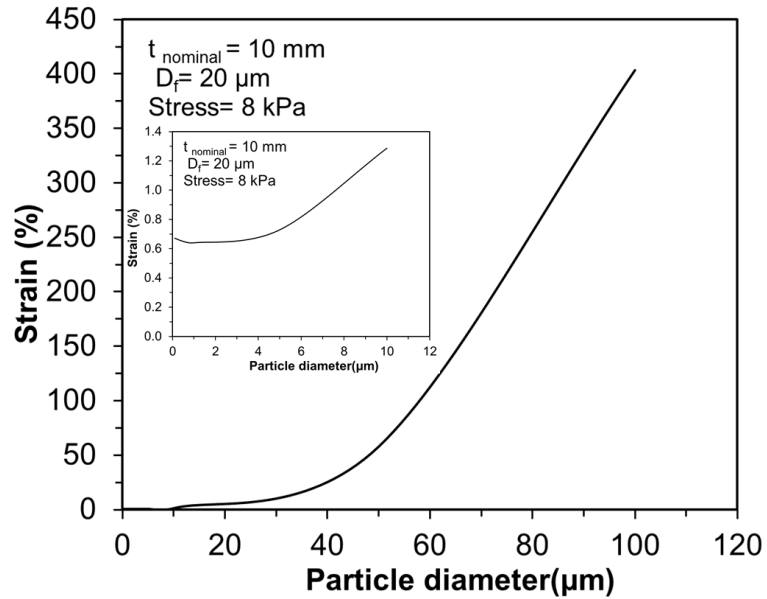


Figure 34. Effect of aerogel particle size on aerogel blanket strain

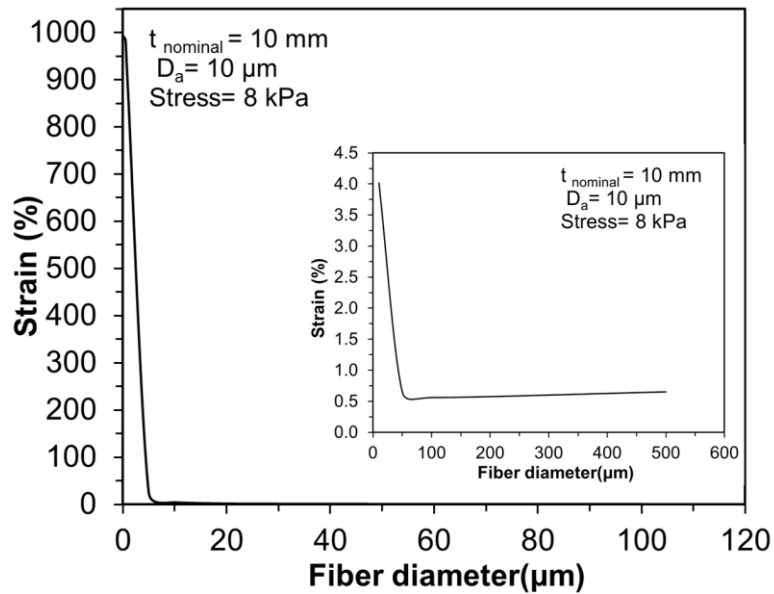


Figure 35. Effect of fiber diameter on aerogel blanket strain

Additionally, the effects of loading history on strain of the available samples were investigated. Presented in Figure 36, the changes to the materials under repeated loading cycles

between 0.7 to 2 kPa for thinner samples and 0.7 to 5 kPa for thicker ones were subtle, and the responses of the materials to compression became stable after ~5 cycles of mechanical deformation. Hysteresis in the HFM loading-unloading cycles indicated that plastic deformation occurred. This was attributed to the inelastic nature of aerogel blankets, which is a result of rearrangement of the pores after applying uniaxial load on the material. Once the volume of the void spaces is reduced under compression it will not be fully recovered during decompression. Applying 10 compression-decompression cycles decreased the thickness of 10 mm CZ by 6% and the thickness of 8 mm TW by 3.5%. For the 5 mm samples, a thickness reduction of 2% for CZ and 1.5% for TW were observed, respectively.

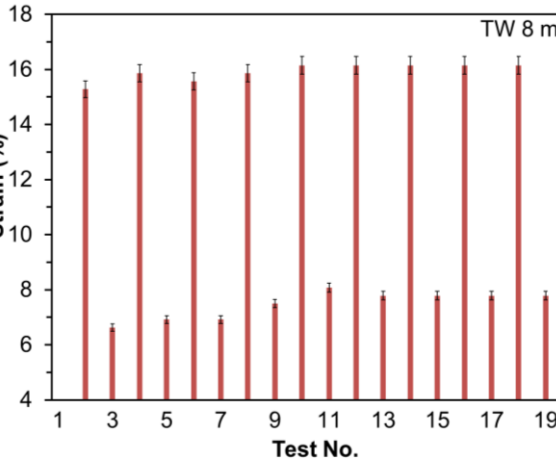
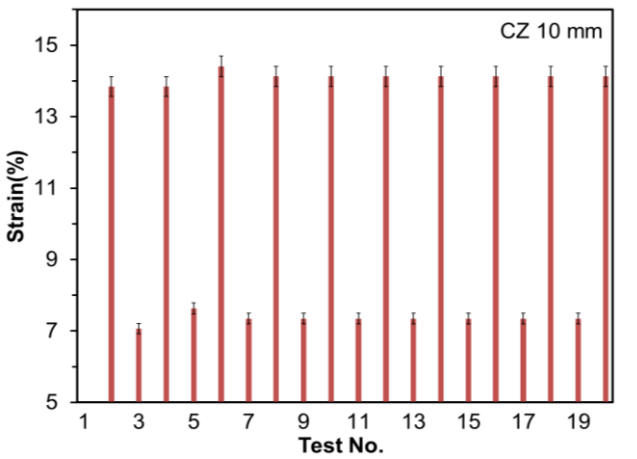
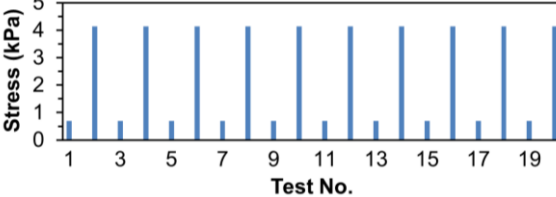
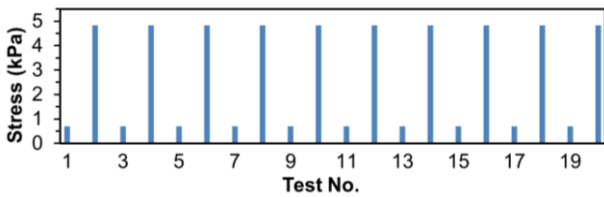
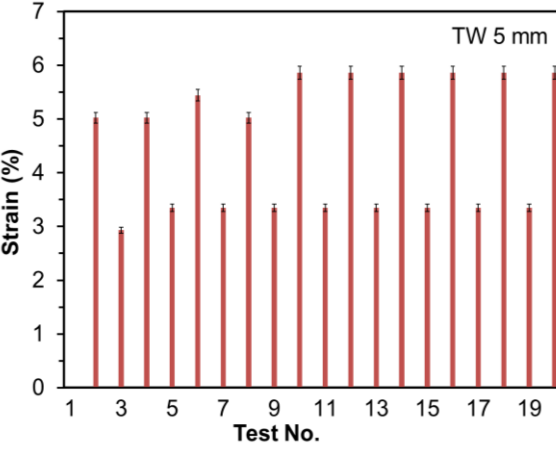
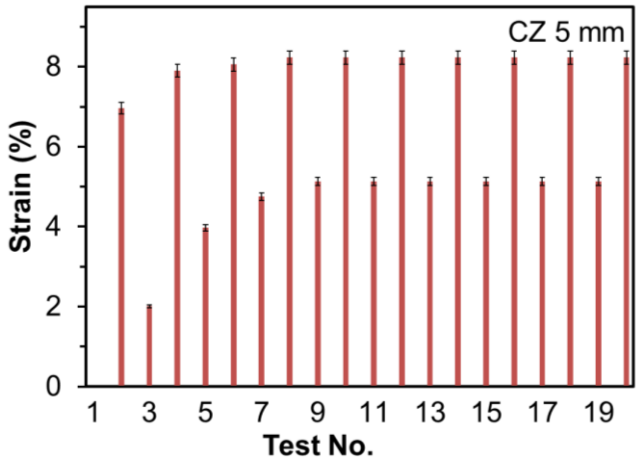
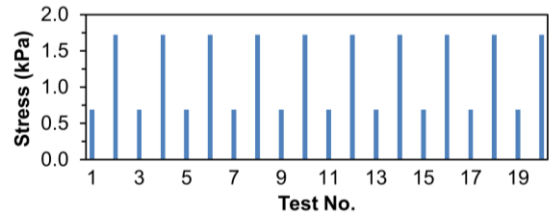
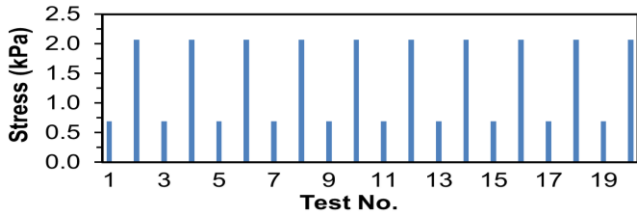


Figure 36. Cycle test for load range of 0.7-2 kPa for thinner samples and 0.7-5 kPa for thicker ones

Chapter 4.

Combined Thermal and Mechanical Deformation Analysis of Aerogel Blankets

Aerogel blankets can be used in a variety of enclosures and are greatly relied upon for their very low thermal conductivity. However, the low thermal conductivity increases if the material gets compressed, the temperature or humidity increases and the intended thermal performance cannot be achieved anymore. Hence, it is essential to consider similar conditions in modeling the thermal properties of aerogel blankets. In this chapter, the combined effects of T, RH and deformation are studied on the thermal resistance (R-value) variation of aerogel blankets and the major results are published in the Journal of Energy and Buildings[102]. The experimental studies as well as developing the analytical model were performed by the author of the thesis.

4.1. The Present Model

The relationship for predicting the deformation of aerogel blanket samples under uniaxial compression from section 3.1 can be extended to predict the thermal resistance of the samples at various compressions. The relationship between the thermal resistance, thickness, and effective thermal conductivity is as follows:

$$R = \frac{t_{b,i}}{k_{eff}} \quad i = 1, 2 \quad (55)$$

In Eq. (55), the thickness of the sample can be calculated by having the analytical model of deformation and porosity of the material at each level of loading (Eq.(53)) and the thermal conductivity as a function of temperature and porosity using Eq.(39), following section 2.2, at dry and humid conditions. The two analytical models for predicting the deformation and thermal conductivity are coupled through the mutual important parameter of porosity (Figure 37). Therefore, both of them should be solved simultaneously so that the predicted k-value (or accordingly R-value) displays the effect of the updated porosity at each T, RH and compression condition.

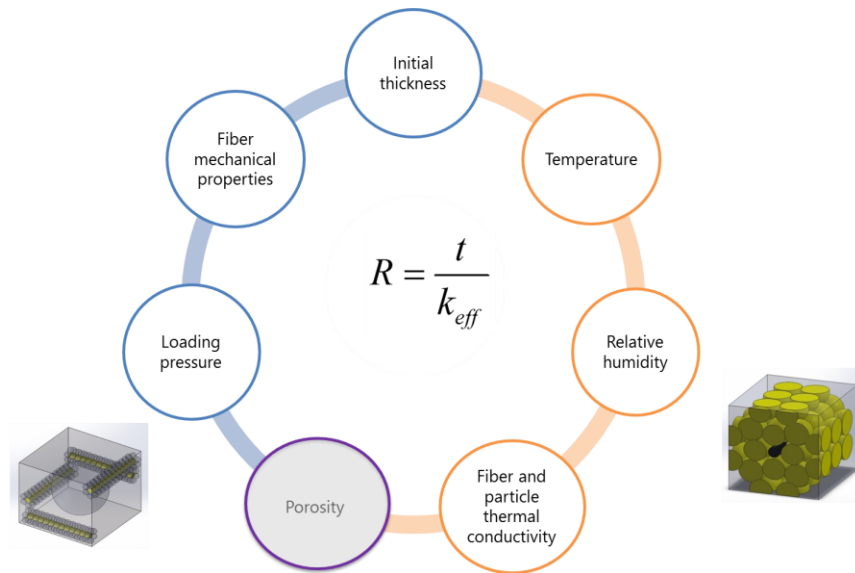


Figure 37. Thermal resistance modeling methodology

4.2. Experimental Study

The thermal resistance of typical insulation materials decreases with compression. Therefore, it is essential to control sample compression during thermo-physical property testing. In this section, HFM was employed to measure the thermal resistance (R -value) of aerogel blankets over a range of compression. The maximum load that HFM can apply on samples depends on two factors: 1) the compression load cannot be greater than 21 kPa; 2) the combined thickness of the specimen, the heat flux transducer, and any damping material, which in total equals the distance between the cold and hot plates, must be controlled to be large enough in order to minimize the effect of edge losses on the measurement of heat flux [18]. In this study, insulation samples (30.5 cm×30.5 cm) were tested between two heat flux sensors under a specific temperature gradient, applied by a hot plate and cold plate. Each specimen was tested under increasing loads to the minimum allowed sample thickness. The total thermal resistance was calculated from the equilibrium temperature difference across the sample and the known heat flux applied to the sample. Further details of the apparatus and the methodology used in the thermal resistance measurements can be found in ASTM C518[100].

4.3. Results and Discussion

Series of measurements were performed using HFM to study the variation of samples thermal resistances as a function of their thicknesses as shown in Figure 38. A linear relationship

between total thermal resistance and thickness shows that the thermal conductivity remains almost constant during compression and porosity variation at different levels of loading is not prominent.

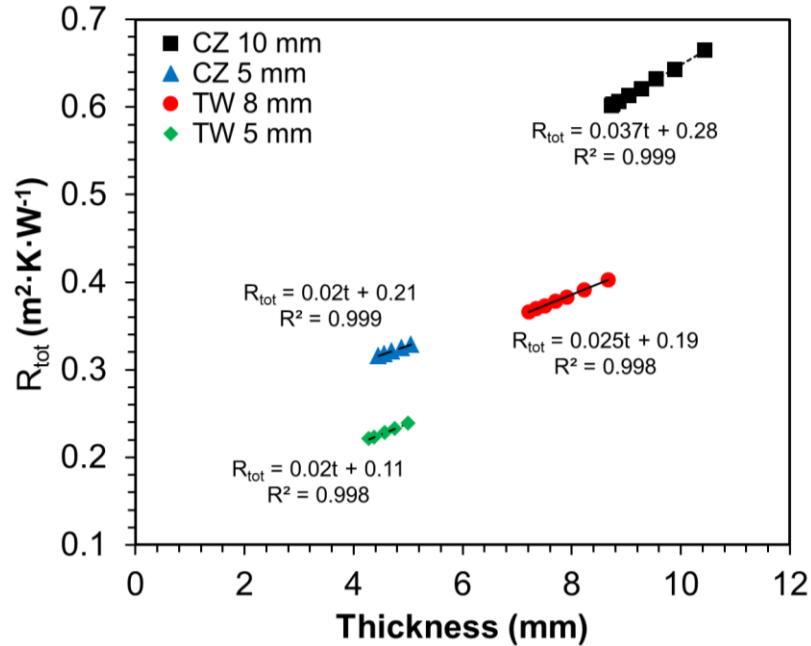


Figure 38. Total resistance variation as a function of thickness at T=25°C and RH=0%.

Figure 39 and Figure 40 demonstrate the variation of resistance as a function of compressive load for four different samples. The error bars represent the standard deviation of the three measurements that were performed to obtain each data point. The R-values were obtained at reduced thicknesses as a function of compression without removing the insulation specimen from the HFM. Results show that when the compression load was increased from 0.7 to 4.5 kPa, the resistance decreased 8.5% for CZ and 9% for TW for samples with 5 mm thickness. These values for samples with higher thicknesses were 10% and 8.5% for CZ and TW, respectively. Less thickness under mechanical pressure results in lower R-value in both materials and it can be concluded that resistance reduction in aerogel blanket insulation can be as high as 10% under ~7 kPa compression, which is only due to mechanical deformation, *i.e.*, thickness reduction. The resistance reduction from full thickness condition of 30 cm for rock wool, cellulose, and fiberglass after applying just about 0.14 kPa load were shown to be 20%, 23%, and 20%, respectively [51], which is much greater than the thermal resistance loss that occurs for aerogel blanket under similar condition. Hence, aerogel blankets are remarkably more efficient thermal insulation materials in terms of thermal performance, space occupation (considering the required

thickness of conventional insulations for having almost the same thermal resistance as aerogel blankets), deformation and thermal resistance loss under compression.

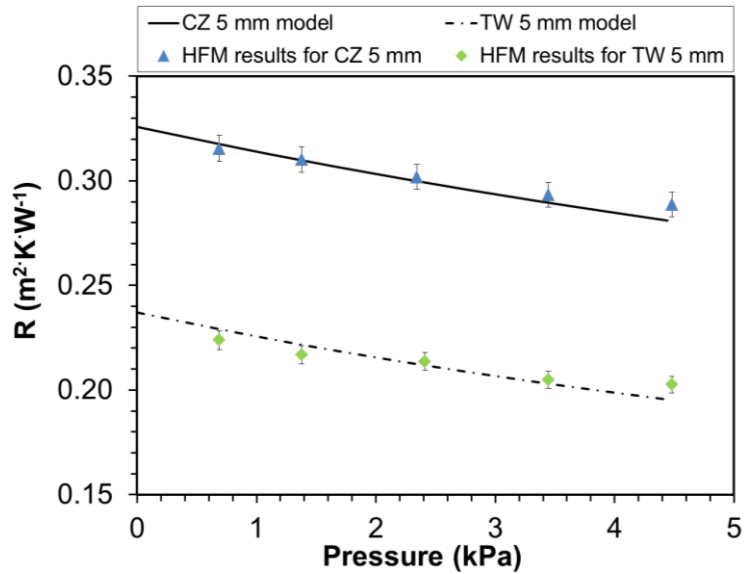


Figure 39. Resistance variation of CZ of 5 mm nominal thickness and TW of 5 mm nominal thickness at various compressive loads at T=25°C and RH=0%.

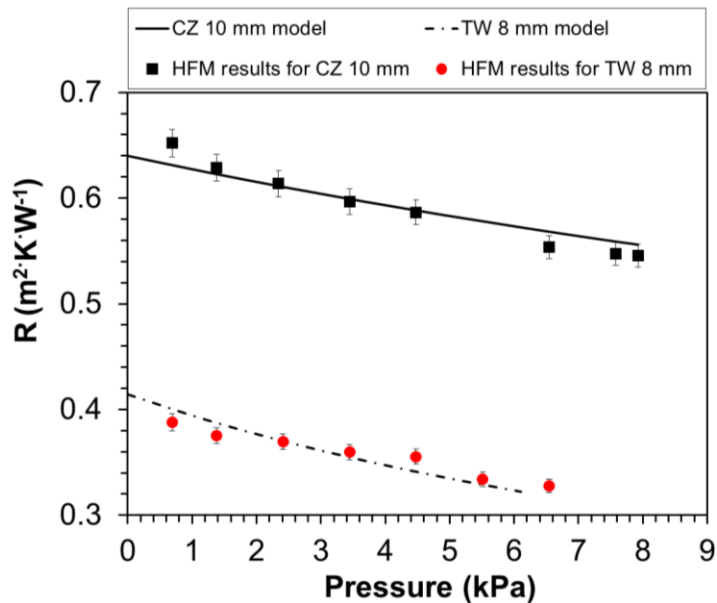


Figure 40. Resistance variation of CZ of 10 mm nominal thickness and TW of 8 mm nominal thickness at various compressive loads at T=25°C and RH=0%.

The effects of temperature and relative humidity variation on the bulk thermal resistance of aerogel blankets as a function of the applied pressure can also be calculated using the unified

analytical model for predicting the R-value of aerogel blankets. The results of RH variation and T variation on R-value of 5 mm CZ are presented in Figure 41 and Figure 42 as a sample results to show how the unified model works. The results also prove that increasing mechanical load, T and RH are all the factors that lead to R-value reduction of aerogel blanket insulation and are required to be well designed to have this super insulation material at its ideal, expected condition.

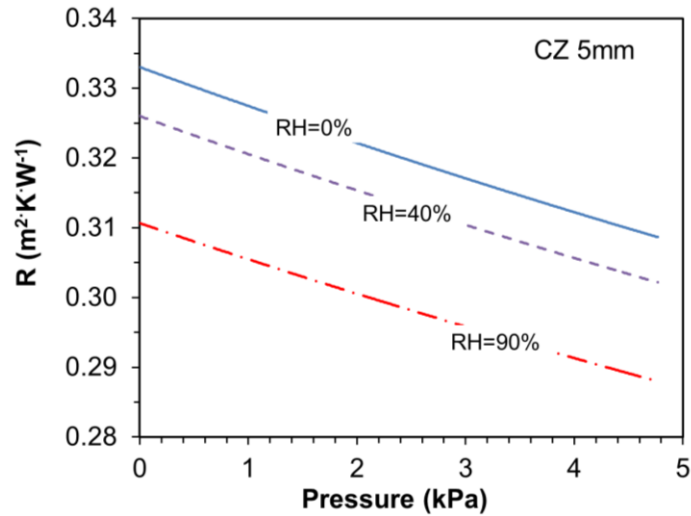


Figure 41. Resistance variation of CZ of 5 mm nominal thickness at various compressive loads at $T=25^{\circ}\text{C}$ and changing RH.

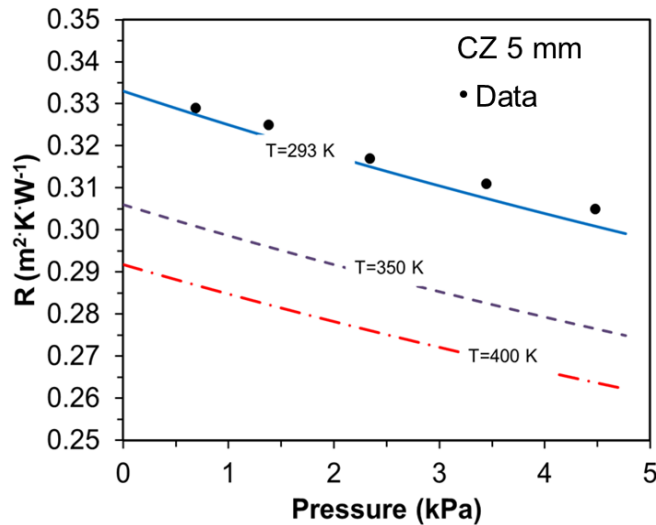


Figure 42. Resistance variation of CZ of 5 mm nominal thickness at various compressive loads at $\text{RH}=0\%$ and changing temperature. The data are experimental results from HFM.

Chapter 5.

Summary and Future Work

In this thesis, an experimental and theoretical study of the thermal and mechanical performance of aerogel blankets were performed considering the effect of temperature and moisture content at transient and steady-state conditions as well as deformation under uniaxial compression. Although each effect was modeled separately, they are all based on mutual assumptions and followed the same method, which is the unit cell approach. Defining identical geometry in the analytical models gave us the option of connecting them together in order to analyse a material by one analytical modeling package. In other words, having specifications of an aerogel blanket such as fiber diameter, fiber thermal conductivity, porosity, and average pore size as inputs of the model, one can obtain the R-value of the sample under defined T, RH and mechanical pressure. The following paragraphs summarize the research and findings of this thesis.

Material characterizations such as porosimetry, spectroscopy and imaging were performed on two types of commercially available aerogel blankets named Cryogel[®]Z (CZ) and Thermalwrap[™] (TW). Mercury intrusion porosimetry (MIP) of the samples provided the value of their porosity, SEM image analysis provided the required modeling inputs such as fiber and particle diameters and the average pore sizes. Fourier Transform Infrared spectroscopy also was used to measure the transmittance of the materials to obtain extinction coefficients. Extinction coefficients are required for modeling the radiation heat transfer in aerogel blankets and can be modeled with more details, which would be a nice addition to this work. Having prepared the infrastructure, an analytical model was developed for predicting the effective thermal conductivity of aerogel blankets as a function of temperature and relative humidity (RH). This model accounted for solid and gas conduction as well as radiation, and was validated with experimental data from heat flow meter (HFM) under dry conditions (RH=0%) and transient plane source (TPS) under different levels of humidity. The temperature study of aerogel blankets showed that their effective thermal conductivity is lower than that of many other conventional types of insulation materials in a wide range of temperatures. Also, increasing temperature for 100°C at dry conditions results in increasing the effective thermal conductivity by approximately 10% for CZ samples and 30% for TW samples. A thermal performance study of aerogel blankets at cyclic conditions of temperature showed that temperature cycling has no hysteresis effect on k-value of

aerogel blankets although at each cycle by changing the temperature, thermal conductivity change happened.

In order to model the effect of moisture on the effective thermal conductivity of aerogel blankets moisture accumulation in two aerogel blanket samples were measured as a function of RH and temperature. The results showed that CZ can hold less moisture compared to TW samples at the same condition and moisture content of both samples increases at higher RH and lower temperature. These highly sensitive measurements (maximum of 2.5% moisture content for CZ and 3% moisture content for TW) were performed using an accurate scale outside of the environmental chamber. For future studies, it is better to set up a test bed inside the environmental chamber to measure the weight changes continuously, when the material is actually under the desired condition. For thermal conductivity measurements at various RH conditions, the setup of TPS-humidifier assembly was designed. Experimental study of aerogel blankets at steady-state condition (24 hours rest time after applying the humidity condition to the TPS chamber) using TPS-humidifier assembly revealed that the effective thermal conductivity of the investigated samples increases by increasing RH. This increase is 13.5% and 11.5% for CZ at 25°C and 45°C, respectively and 11.8% and 9.3% for TW at 25°C and 45°C, respectively. This trend can be explained by considering the higher thermal conductivity of the inbuilt moisture compared to dry air as the filling fluid inside the pores. Also, more k-value increase at lower temperatures is the result of having more moisture content at lower temperatures.

In order to study the effect of moisture content at transient regime, thermal conductivity cyclic tests performed using TPS-humidifier assembly. The results showed that it took approximately three cycles, of 5 hours rest time, till the effective thermal conductivity reaches its maximum, which means that the material was holding all the moisture that it could. Therefore, material is showing some resistance against diffusion of moisture and limited capacitance for storing the moisture inside the pores. Based on these findings, a new moisture diffusion model was introduced using the concept of RC circuit, based on the analogy between electrical and mass transfer phenomena. This model was integrated into the analytical model of thermal conductivity as a function of temperature to include the effect of moisture diffusion on thermal conductivity of aerogel blankets. Long term studies of k-value under three RH conditions inside TPS chamber were performed to calculate the diffusion coefficient of CZ aerogel blanket. The same study can be done on TW as well, which we did not have enough time to do. Moreover, the actual measurement of diffusion coefficient of aerogel blanket samples would be a useful addition to this study. The analytical model can also be upgraded to a more advanced model by adding

pore size distribution and adsorbed water distribution inside the pores. Condensation can be studied separately to include both concentration and temperature gradient effects on moisture diffusion, which is suggested for future studies of aerogel blankets. Also, studying the effect of liquid water freezing inside the pores on thermal and mechanical performance of aerogel blankets at sub-ambient applications would be a valuable addition to this study.

For modeling the effect of uniaxial compression on mechanical deformation of aerogel blanket samples, an extended version of the T and RH unit cell was used. The analytically predicted deformation of aerogel blanket under compression matched well with the experimental results from tests performed with the HFM and thermomechanical analyzer (TMA). The modeling and experimental results indicated that the aerogel blanket is a mechanically strong material showing less than 14% strain for thinner samples and less than 24% strain for thicker samples of CZ and TW after applying maximum possible load on them, which put them in grade I insulation class compared to conventional thermal insulations. During mechanical performance study of aerogel blankets at cyclic conditions of compression/decompression hysteresis effects were observed, which are due to the inelastic nature of aerogel blankets although the deformation was relatively small.

Long-term measurements of the effect of mechanical loading on the samples can be done (creep tests) to study the degradation process of the material under compression.

In the last chapter, the variation of R-value of aerogel blankets as a result of T, RH and compression were investigated mathematically and experimentally. The analytical models for predicting the thermal conductivity and deformation of aerogel blankets were coupled to provide a package that is able to predict the R-value of aerogel blankets under varying operating conditions of T, RH and compression. Modeling and tests results showed small variation of R-value by increasing the mechanical load on the materials, <9% for thinner samples and <16% for thicker ones at 25°C and 0% RH. These results indicate that aerogel blankets remain remarkably effective even under compression. However, increasing the mechanical load on the material, T and RH condition are all the factors that lead to R-value reduction of aerogel blanket insulation and are required to be well designed to have this super insulation material at its ideal, expected condition. Investigation of the effect of compression under different humidity and temperature conditions, experimentally, would be a valuable verification for this model, which can be done in future.

Optimization study should be done to design more efficient and cost-effective aerogel blankets, which is the ultimate objective for developing such analytical models.

References

- [1] D. Ürge-Vorsatz, L. F. Cabeza, S. Serrano, C. Barreneche, and K. Petrichenko, "Heating and cooling energy trends and drivers in buildings," *Renew. Sustain. Energy Rev.*, vol. 41, pp. 85–98, 2015.
- [2] International Energy Agency, "Transition to Sustainable Buildings," 2013.
- [3] L. Pérez-Lombard, J. Ortiz, and C. Pout, "A review on buildings energy consumption information," *Energy Build.*, vol. 40, no. 3, pp. 394–398, 2008.
- [4] O. C. Perez, "The behavior of aerogel blankets as insulation material in external walls at high temperatures," Chalmers university of technology, 2012.
- [5] Energy Information Administration, *International Energy Outlook*, vol. 484, no. June. 2006.
- [6] L. F. Cabeza, A. Castell, M. Medrano, I. Martorell, G. Pérez, and I. Fernández, "Experimental study on the performance of insulation materials in Mediterranean construction," *Energy Build.*, vol. 42, no. 5, pp. 630–636, 2010.
- [7] A. A. Abdou and I. M. Budaiwi, "Comparison of Thermal Conductivity Measurements of Building Insulation Materials under Various Operating Temperatures," *J. Build. Phys.*, vol. 29, no. 2, pp. 171–184, 2005.
- [8] B.-M. Zhang, S.-Y. Zhao, and X.-D. He, "Experimental and theoretical studies on high-temperature thermal properties of fibrous insulation," *J. Quant. Spectrosc. Radiat. Transf.*, vol. 109, no. 7, pp. 1309–1324, 2008.
- [9] A.-L. Pasanen, S. Rautiala, J. P. Kasanen, P. Raunio, J. Rantamäki, and P. Kalliokoski, "The relationship between measured moisture conditions and fungal concentrations in water-damaged building materials.," *Indoor Air*, vol. 10, no. 2, pp. 111–120, 2000.
- [10] K. Huttunen, H. Rintala, M. R. Hirvonen, A. Vepsäläinen, A. Hyvärinen, T. Meklin, M. Toivola, and A. Nevalainen, "Indoor air particles and bioaerosols before and after renovation of moisture-damaged buildings: The effect on biological activity and microbial flora," *Environ. Res.*, vol. 107, no. 3, pp. 291–298, 2008.

- [11] J. Lstiburek, N. Yost, and T. Brennan, "Mold: Causes, Health Effects and Clean-Up," 2002.
- [12] J. Fan and X. Wen, "Modeling heat and moisture transfer through fibrous insulation with phase change and mobile condensates," *Int. J. Heat Mass Transf.*, vol. 45, no. 19, pp. 4045–4055, Sep. 2002.
- [13] J. Fan and X. X. Wen, "An improved model of heat and moisture transfer with phase change and mobile condensates in fibrous insulation and comparison with experimental results," *Int. J. Heat Mass Transf.*, vol. 47, no. 10–11, pp. 2343–2352, May 2004.
- [14] F. Björk and T. Enochsson, "Properties of thermal insulation materials during extreme environment changes," *Constr. Build. Mater.*, vol. 23, no. 6, pp. 2189–2195, 2009.
- [15] "Thermal insulation products for buildings — Factory made mineral wool (MW) products — Specification," Wien, 2009.
- [16] T. Vrana, "Impact of Moisture on Long Term Performance of Insulating Products," KTH – The Royal Institute of Technology, 2007.
- [17] H. Maleki, L. Durães, and A. Portugal, "An overview on silica aerogels synthesis and different mechanical reinforcing strategies," *J. Non. Cryst. Solids*, vol. 385, pp. 55–74, 2014.
- [18] G. W. Brinker, C. J.; Scherer, *Sol-Gel Science*. 1990.
- [19] E. Cuce, P. M. Cuce, C. J. Wood, and S. B. Riffat, "Toward aerogel based thermal superinsulation in buildings: A comprehensive review," *Renew. Sustain. Energy Rev.*, vol. 34, pp. 273–299, Jun. 2014.
- [20] J. Ryu, "Flexible aerogel superinsulation and its manufacture," 6,068,882.
- [21] G. Wei, X. Zhang, and F. Yu, "Effective thermal conductivity analysis of xonotlite-aerogel composite insulation material," *J. Therm. Sci.*, vol. 18, no. 2, pp. 142–149, May 2009.
- [22] J. M. S. F. Rouanet, R. K. Massey, "Aerogel containing blanket," 7635411 B2, 2009.
- [23] R. and A.-C. E. American Society of Heating, *ASHRAE Handbook: Fundamentals*, SI

Edition. Atlanta, Ga: American Society of Heating Refrigerating and Air-Conditionin, 2005.

- [24] D. P. Rizzetta, M. R. Visbal, M. J. Stanek, G. R. Cunnington, and S. C. Lee, "Radiative properties of fibrous insulations - Theory versus experiment," *J. Thermophys. Heat Transf.*, vol. 10, no. 3, pp. 460–466, 1996.
- [25] S.-C. Lee and G. R. Cunnington, "Conduction and Radiation Heat Transfer in High-Porosity Fiber Thermal Insulation," *J. Thermophys. Heat Transf.*, vol. 14, no. 2, pp. 121–136, Apr. 2000.
- [26] Kyung Wha Oh and S. H. K. Kim, "Ultra-porous flexible PET/Aerogel blanket for sound absorption and thermal insulation," *Fibers Polym.*, vol. 10, no. 5, pp. 731–737, Nov. 2009.
- [27] J. Wang, J. Kuhn, and X. Lu, "Monolithic silica aerogel insulation doped with TiO₂ powder and ceramic fibers," *J. Non. Cryst. Solids*, vol. 186, no. 95, pp. 296–300, 1995.
- [28] G. Wei, Y. Liu, X. Zhang, F. Yu, and X. Du, "Thermal conductivities study on silica aerogel and its composite insulation materials," *Int. J. Heat Mass Transf.*, vol. 54, no. 11–12, pp. 2355–2366, 2011.
- [29] G. Lu, X. D. Wang, Y. Y. Duan, and X. W. Li, "Effects of non-ideal structures and high temperatures on the insulation properties of aerogel-based composite materials," *J. Non. Cryst. Solids*, vol. 357, no. 22–23, pp. 3822–3829, 2011.
- [30] G. Wei, Y. Liu, X. Zhang, F. Yu, and X. Du, "Thermal conductivities study on silica aerogel and its composite insulation materials," *Int. J. Heat Mass Transf.*, vol. 54, no. 11–12, pp. 2355–2366, May 2011.
- [31] R. Coquard, D. Baillis, V. Grigorova, F. Enguehard, D. Quenard, and P. Levitz, "Modelling of the conductive heat transfer through nano-structured porous silica materials," *J. Non. Cryst. Solids*, vol. 363, pp. 103–115, Mar. 2013.
- [32] J. B. Alvey, "performance of aerogel composite and foam insulations," University of Illinois at Urbana-Champaign, 2014.
- [33] T. Xie, Y.-L. He, and Z.-J. Hu, "Theoretical study on thermal conductivities of silica aerogel composite insulating material," *Int. J. Heat Mass Transf.*, vol. 58, no. 1–2, pp. 540–552, Mar. 2013.

- [34] J.-J. Zhao, Y.-Y. Duan, X.-D. Wang, and B.-X. Wang, "Radiative properties and heat transfer characteristics of fiber-loaded silica aerogel composites for thermal insulation," *Int. J. Heat Mass Transf.*, vol. 55, no. 19–20, pp. 5196–5204, Sep. 2012.
- [35] B. T. Chaddock, J. B., "Heat and mass transfer in building materials and structures," in *21st symposium of the International Centre for Heat and Mass Transfer (ICHMT)*, 1991.
- [36] J. C. Alvarez, "Evaluation of Moisture Diffusion Theories in Porous Materials," Virginia Polytechnic Institute and State University In, 1998.
- [37] D. G. Stephenson, "Thermal diffusion of water vapour through glass fibre insulation," in *e-Sim 2004 Conference*, 2004, pp. 1–6.
- [38] Z. Pavlík, L. Fiala, E. Vejmelková, and R. Černý, "Application of effective media theory for determination of thermal properties of hollow bricks as a function of moisture content," *Int. J. Thermophys.*, vol. 34, no. 5, pp. 894–908, 2013.
- [39] Z. Pavlík, E. Vejmelková, L. Fiala, and R. Černý, "Effect of moisture on thermal conductivity of lime-based composites," *Int. J. Thermophys.*, vol. 30, no. 6, pp. 1999–2014, 2009.
- [40] E. Vejmelková, M. Keppert, P. Rovnaníková, Z. Keršner, and R. Černý, "Application of burnt clay shale as pozzolan addition to lime mortar," *Cem. Concr. Compos.*, vol. 34, no. 4, pp. 486–492, 2012.
- [41] A. Karamanos, S. Hاديarakou, and A. M. Papadopoulos, "The impact of temperature and moisture on the thermal performance of stone wool," *Energy Build.*, vol. 40, no. 8, pp. 1402–1411, 2008.
- [42] A. Abdou and I. Budaiwi, "The variation of thermal conductivity of fibrous insulation materials under different levels of moisture content," *Constr. Build. Mater.*, vol. 43, pp. 533–544, 2013.
- [43] M. Jerman and R. Černý, "Effect of moisture content on heat and moisture transport and storage properties of thermal insulation materials," *Energy Build.*, vol. 53, pp. 39–46, 2012.
- [44] F. Ochs, W. Heidemann, and H. Müller-Steinhagen, "Effective thermal conductivity of

- moistened insulation materials as a function of temperature,” *Int. J. Heat Mass Transf.*, vol. 51, no. 3–4, pp. 539–552, 2008.
- [45] O. Krischer and W. Kast, “Die wissenschaftlichen Grundlagen der Trocknungstechnik,” *Springer*, 1992.
- [46] Á. Lakatos, “Investigation of the moisture induced degradation of the thermal properties of aerogel blankets: Measurements, calculations, simulations,” *Energy Build.*, vol. 139, pp. 506–516, 2017.
- [47] R. Galliano, K. Ghazi Wakili, T. Stahl, B. Binder, and B. Daniotti, “Performance evaluation of aerogel-based and perlite-based prototyped insulations for internal thermal retrofitting: HMT model validation by monitoring at demo scale,” *Energy Build.*, vol. 126, pp. 275–286, 2016.
- [48] T. Stahl, S. Brunner, M. Zimmermann, and K. Ghazi Wakili, “Thermo-hygric properties of a newly developed aerogel based insulation rendering for both exterior and interior applications,” *Energy Build.*, vol. 44, pp. 114–117, Jan. 2012.
- [49] T. Ihara, B. P. Jelle, T. Gao, and A. Gustavsen, “Aerogel granule aging driven by moisture and solar radiation,” *Energy Build.*, vol. 103, pp. 238–248, 2015.
- [50] K. Ghazi Wakili, T. Stahl, E. Heiduk, M. Schuss, R. Vonbank, U. Pont, C. Sustr, D. Wolosiuk, and A. Mahdavi, “High performance aerogel containing plaster for historic buildings with structured façades,” *Energy Procedia*, vol. 78, no. 0, pp. 949–954, 2015.
- [51] D. W. Yarbrough and J. ti. Wright, “Reduction in the thermal resistance of loose fill insulation and fiberglass batts due to compression,” Cookeville, Tennessee, 1981.
- [52] R. D. Adams and J. G. Hust, “A round robin on apparent thermal conductivity of several loose-fill insulations,” *Insul. Mater. Test. Appl. ASTM STP 1030*, pp. 263–289, 1990.
- [53] R. S. Graves and D. W. Yarbrough, “The effect of compression on the material R -Value of fiberglass batt Insulation,” *J. Therm. Insul.*, vol. 15, pp. 248–260, 1992.
- [54] J. G. Symons and V. Clarke, R. E. ClarkePeirce, “The thermal performance of several Australian fibrous insulating materials,” *Therm. Insul. bldg. Envs.*, vol. 19, no. July, pp. 72–88, 1995.

- [55] M. Kolich, P. Hoke, D. Dooge, M. Doroudian, E. Litovsky, and J. Kleiman, "Influence of temperature and mechanical compression on thermophysical properties of car interior foam plastics insulation," *J. Elastomers Plast.*, vol. 46, no. 2, pp. 132–143, 2014.
- [56] E. Cuce, P. M. Cuce, C. J. Wood, and S. B. Riffat, "Optimizing insulation thickness and analysing environmental impacts of aerogel-based thermal superinsulation in buildings," *Energy Build.*, vol. 77, pp. 28–39, 2014.
- [57] N. Gupta and W. Ricci, "Processing and compressive properties of aerogel/epoxy composites," *J. Mater. Process. Technol.*, vol. 198, pp. 178–182, 2008.
- [58] E. R. Bardy, J. C. Mollendorf, and D. R. Pendergast, "Thermal conductivity and compressive strain of aerogel insulation blankets under applied hydrostatic pressure," *J. Heat Transfer*, vol. 129, no. 2, p. 232, 2007.
- [59] D. Shi, Y. Sun, J. Feng, X. Yang, S. Han, C. Mi, Y. Jiang, and H. Qi, "Experimental investigation on high temperature anisotropic compression properties of ceramic-fiber-reinforced SiO₂ aerogel," *Mater. Sci. Eng. A*, vol. 585, pp. 25–31, 2013.
- [60] H. Wu, Y. Liao, Y. Ding, H. Wang, C. Peng, and S. Yin, "Engineering thermal and mechanical properties of multilayer aligned fiber-reinforced aerogel composites," *Heat Transf. Eng.*, vol. 35, no. 11–12, pp. 1061–1070, 2014.
- [61] a Tamayol and M. Bahrami, "Numerical investigation of flow in fibrous porous media," no. September, pp. 21–26, 2008.
- [62] a. Tamayol, K. W. Wong, and M. Bahrami, "Effects of microstructure on flow properties of fibrous porous media at moderate Reynolds number," *Phys. Rev. E*, vol. 85, no. January 2011, pp. 1–7, 2012.
- [63] E. Sadeghi, M. Bahrami, and N. Djilali, "Analytic determination of the effective thermal conductivity of PEM fuel cell gas diffusion layers," *J. Power Sources*, vol. 179, no. 1, pp. 200–208, Apr. 2008.
- [64] X. H. Yang, J. J. Kuang, T. J. Lu, F. S. Han, and T. Kim, "A simplistic analytical unit cell based model for the effective thermal conductivity of high porosity open-cell metal foams," *J. Phys. D. Appl. Phys.*, vol. 46, no. 25, p. 255302, Jun. 2013.

- [65] W. van Antwerpen, P. G. Rousseau, and C. G. du Toit, "Multi-sphere Unit Cell model to calculate the effective thermal conductivity in packed pebble beds of mono-sized spheres," *Nucl. Eng. Des.*, vol. 247, pp. 183–201, Jun. 2012.
- [66] C. T. HSU, P. CHENG, and K. W. Wong, "Modified Zehner-Schlunder models for stagnant thermal conductivity of porous media," *Heat mass Transf.*, vol. 31, no. 17, pp. 2751–2759, 1994.
- [67] A. Hoseini, C. McCague, M. Andisheh-Tadbir, and M. Bahrami, "Aerogel blankets: From mathematical modeling to material characterization and experimental analysis," *Int. J. Heat Mass Transf.*, vol. 93, pp. 1124–1131, 2016.
- [68] A. Hoseini and M. Bahrami, "Effects of humidity on thermal performance of aerogel insulation blankets," *J. Build. Eng.*, vol. 13, no. July, pp. 107–115, 2017.
- [69] A. Ahern, G. Verbist, D. Weaire, R. Phelan, and H. Fleurent, "The conductivity of foams: a generalisation of the electrical to the thermal case," *Colloids Surfaces A Physicochem. Eng. Asp.*, vol. 263, no. 1–3, pp. 275–279, 2005.
- [70] G. Wei, Y. Liu, X. Zhang, F. Yu, and X. Du, "Thermal conductivities study on silica aerogel and its composite insulation materials," *Int. J. Heat Mass Transf.*, vol. 54, no. 11–12, pp. 2355–2366, May 2011.
- [71] J. H. Vansant, *Conduction heat transfer solutions*, no. March. 1980.
- [72] L. Huang, "Feasibility study of using silica aerogel as insulation for buildings," KTH University, 2012.
- [73] G. B. a. Carotenuto, "the Effective Thermal Conductivity of Packed Beds of Spheres for a Finite Contact Area," *Numer. Heat Transf. Part A Appl.*, vol. 37, no. 4, pp. 343–357, Mar. 2000.
- [74] G. Buonanno, a. Carotenuto, G. Giovinco, and N. Massarotti, "Experimental and Theoretical Modeling of the Effective Thermal Conductivity of Rough Steel Spheroid Packed Beds," *J. Heat Transfer*, vol. 125, no. 4, p. 693, 2003.
- [75] N. M. G. Buonanno, A. Carotenuto, G. Giovinco and Sarotti, "Effective thermal conductivity of rough spheres packed beds," in *Proceedings of HT2003, ASME Heat*

Transfer Conference, 2003.

- [76] Y. Ogniewicz and M. M. Yovanovich, "Effective conductivity of regularly packed spheres: basic cell model with constriction," in *L.S. Fletcher (Ed.), Heat Transfer and Thermal Control Systems*, 1987.
- [77] P. J. Turyk and M. M. Yovanovich, "Modified effective conductivity models for basic cells of simple cubic packed beds," in *Proc. 23rd National Heat Transfer Conference*, 1985, pp. 9–19.
- [78] M. Bahrami, M. M. Yovanovich, and J. R. Culham, "Effective thermal conductivity of rough spherical packed beds," *Int. J. Heat Mass Transf.*, vol. 49, no. 19–20, pp. 3691–3701, Sep. 2006.
- [79] G. Wei, Y. Liu, X. Du, and X. Zhang, "Gaseous Conductivity Study on Silica Aerogel and Its Composite Insulation Materials," *J. Heat Transfer*, vol. 134, no. 4, p. 41301, 2012.
- [80] J.-S. Kwon, C. H. Jang, H. Jung, and T.-H. Song, "Effective thermal conductivity of various filling materials for vacuum insulation panels," *Int. J. Heat Mass Transf.*, vol. 52, no. 23–24, pp. 5525–5532, Nov. 2009.
- [81] S. Jennings, "The Mean Free Path in Air," *J. Aerosol Sci.*, vol. 19, no. 2, pp. 159–166, 1988.
- [82] P. Noiying, M. Hinaje, P. Thounthong, S. Raël, and B. Davat, "Using electrical analogy to describe mass and charge transport in PEM fuel cell," *Renew. Energy*, vol. 44, pp. 128–140, 2012.
- [83] J. N. Davidson, D. A. Stone, M. P. Foster, and C. R. Gould, "Prediction of device temperatures in an electric vehicle battery charger system by analysis of device thermal cross-coupling," *2013 15th Eur. Conf. Power Electron. Appl. EPE 2013*, 2013.
- [84] J. N. Davidson, D. A. Stone, and M. P. Foster, "Required Cauer network order for modelling of thermal transfer impedance," *Electron. Lett.*, vol. 50, no. 4, pp. 1–2, 2014.
- [85] K. Murthy and R. Bedford, "Transformation between Foster and Cauer equivalent networks," *IEEE Trans. Circuits Syst.*, vol. 25, no. 4, pp. 238–239, 1978.

- [86] A. Gholami, M. Ahmadi, and M. Bahrami, "A New Analytical Approach for Dynamic Modeling of Passive Multicomponent Cooling Systems," *J. Electron. Packag.*, vol. 136, no. 3, p. 31010, 2014.
- [87] M. Becherif, D. Hissel, S. Gaagat, and M. Wack, "Electrical equivalent model of a proton exchange membrane fuel cell with experimental validation," *Renew. Energy*, vol. 36, no. 10, pp. 2582–2588, 2011.
- [88] A. Hernandez, D. Hissel, and R. Outbib, "Modeling and fault diagnosis of a polymer electrolyte fuel cell using electrical equivalent analysis," *IEEE Trans. Energy Convers.*, vol. 25, no. 1, pp. 148–160, 2010.
- [89] P. R. Pathapati, X. Xue, and J. Tang, "A new dynamic model for predicting transient phenomena in a PEM fuel cell system," *Renew. Energy*, vol. 30, no. 1, pp. 1–22, 2005.
- [90] K. J. Runtz and M. D. Lyster, "Fuel cell equivalent circuit models for passive mode testing and dynamic mode design," *Can. Conf. Electr. Comput. Eng.*, vol. 2005, no. May, pp. 794–797, 2005.
- [91] A. S. Morris, *Measurement and instrumentation principles*, 3rd ed. Oxford: Butterworth-Heinemann, 2001.
- [92] J. C. Maxwell, *A TREATISE ON ELECTRICITY AND MAGNETISM*, vol. 1, no. 9. Uonfron MACMILLAN AND CO., 1873.
- [93] Á. Lakatos, "Moisture induced changes in the building physics parameters of insulation materials," *Sci. Technol. Built Environ.*, vol. 22, no. 3, pp. 252–260, 2016.
- [94] J. D. Moreno, "Radiative Transfer and Thermal Performance Levels in Foam Insulation Boardstocks," 1991.
- [95] J. R. Siegel, Robert; Howell, *Thermal Radiation heat transfer*, 3rth ed. Washington, D.C.: Hemisphere publishing Corporation, 1993.
- [96] Aspen aerogels, "Cryogel ® Z data sheet," 2012.
- [97] Cabot Aerogel, "Thermal wrap data sheet," 2011.

- [98] J. P. Nayak and J. Bera, "Preparation of Silica Aerogel by Ambient Pressure Drying Process using Rice Husk Ash as Raw Material," *Trans. Indian Ceram. Soc.*, vol. 68, no. 2, pp. 91–94, 2009.
- [99] ISO22007-2, "Plastics-determination of thermal conductivity and thermal diffusivity-part 2: transient plane heat source (hot disc) method," 2008.
- [100] "ASTM C518-10, Standard test method for steady-state thermal transmission properties by means of the heat flow meter apparatus," ASTM International, West Conshohocken, PA, 2010.
- [101] D. F. García, B. García, and J. C. Burgos, "Determination of moisture diffusion coefficient for oil-impregnated Kraft-paper insulation," *Int. J. Electr. Power Energy Syst.*, vol. 53, no. 1, pp. 279–286, 2013.
- [102] A. Hoseini, A. Malekian, and M. Bahrami, "Deformation and thermal resistance study of aerogel blanket insulation material under uniaxial compression," *Energy Build.*, vol. 130, pp. 228–237, 2016.
- [103] V. Norouzifard and M. Bahrami, "Deformation of PEM fuel cell gas diffusion layers under compressive loading: An analytical approach," *J. Power Sources*, vol. 264, pp. 92–99, 2014.
- [104] L. Waguespack, "Thermomechanical Analysis (TMA Q400EM/Q400 specifications)," 2013.
- [105] "Marketch International Inc." [Online]. Available: <https://mkt-intl.com/materials/aerogel/silica-aerogel/>.
- [106] "AZO Materials." [Online]. Available: <http://www.azom.com/properties.aspx?ArticleID=764>.
- [107] "The engineering toolbox." [Online]. Available: http://www.engineeringtoolbox.com/young-modulus-d_417.html.
- [108] D. Julve, J. Ramos, J. Pérez, and M. Menéndez, "Analysis of mercury porosimetry curves of precipitated silica, as an example of compressible porous solids," *J. Non. Cryst. Solids*, vol. 357, no. 4, pp. 1319–1327, 2011.

[109] R. Pirard, S. Blacher, F. Brouers, and J. P. Pirard, "Interpretation of mercury porosimetry applied to aerogels," *J. Mater. Res.*, vol. 10, no. 8, pp. 2114–2119, 1995.

Appendix A.

Pore size measurement

Mercury intrusion and nitrogen sorption are two techniques widely used to characterize the textural properties of mesoporous materials as data treatment methods [108]. The nitrogen adsorption-desorption isotherm analysis gives a distribution of specific surface area and pore volumes in a wide range of porosities from nanopores to mesopores of diameter smaller than 300 nm. Mercury intrusion porosimetry (MIP) gives information on the structure of the pores. The analysis of the distribution of the specific surface area and the specific pore volume in relation with the pore size from mercury porosimetry data is classically based on Washburn's equation. This equation has been derived on the assumption that the mercury intrudes the pore network [109].

Our results indicated that aerogel blankets have a pore diameter distribution that extends from the nanometer to micrometer range. The problem is that N₂ adsorption method captures the pore size range in which macro pores are not considered. On the other hand, although MIP captures pore size range of 3 nm to 0.1 mm, the very high pressure of mercury crushes the structure of the sample. In Figure A-1 and Figure A-2, the difference between MIP and N₂ adsorption porosimetry can be easily observed. According to our compression measurements using heat flow meter (HFM) (See Section 3.2), the maximum compressive load that, for example, 10 mm CZ was able to tolerate was less than 10 kPa (~1.5 psi). Knowing that the mercury intrusion starts from 1.5 psi pressure, it has been observed experimentally that the structure of the samples was damaged by the high pressure required to intrude small cells. That can be explained by the small value of the Young modulus and the ultimate compressive strength of aerogels. Consequently, Washburn's equation cannot be applied to aerogel blankets and the result of pore size distribution cannot be trusted. Hence, the images from scanning electron microscopy (SEM) were utilized to find the mean pore size of the samples statically, which was about 66 micrometer for CZ and 121 micrometer for TW. The drawback of this technique is related to the fact that it provides only a two-dimensional projection of a three-dimensional structure.

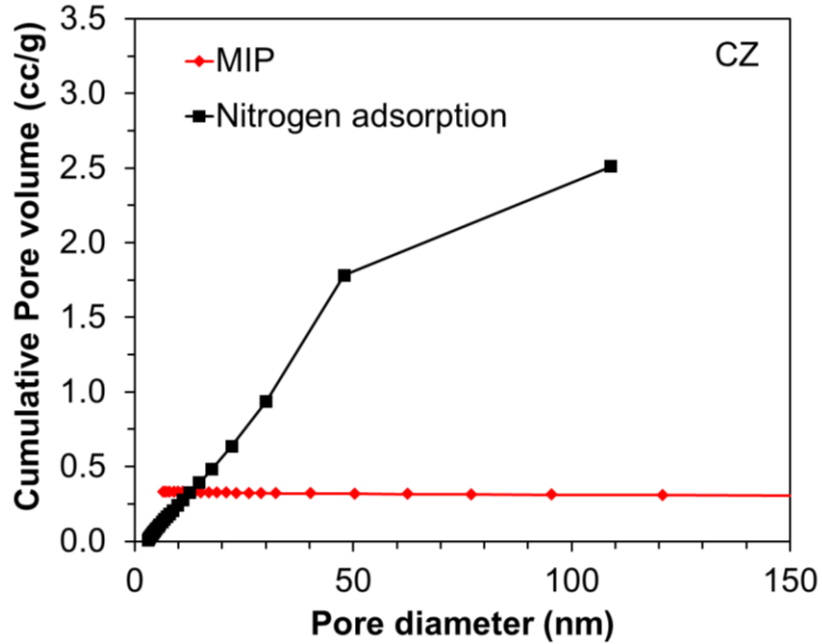


Figure A-1: Cumulative pore volume of 10 mm thick CZ, measured by MIP and N₂ adsorption porosimetry

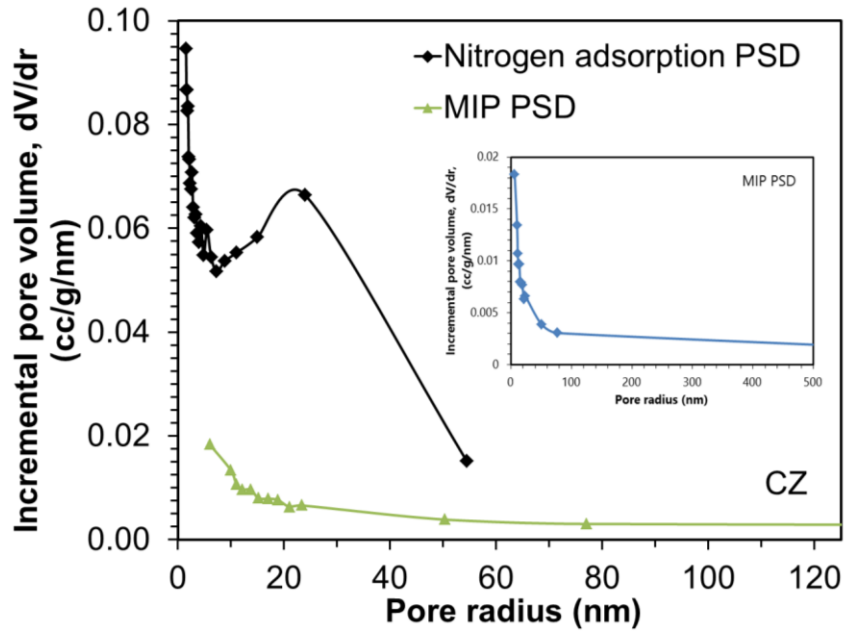


Figure A-2: Incremental pore volume of 10 mm thick CZ, results of MIP and N₂ adsorption porosimetry.

Appendix B.

Experimental data

This appendix contains the experimental data of mechanical and thermal properties of the aerogel blanket samples collected in this research. The samples specifications are reported in Table B-1.

Table B-1: Aerogel blanket samples specifications

Manufacturer Data [60, 61]						
Sample	Provider	Thickness	Density*	Fiber composition	Powder material	Thermal* Conductivity
Cryogel® Z (CZ)	Aspen Aerogel	10±0.5 mm	130 kg·m ⁻³	Polyester/ fiber glass	Silica (SiO ₂)	0.014 W·m ⁻¹ ·K ⁻¹
		5±0.5 mm				
ThermalWrap™ (TW)	Cabot Corp.	8±0.5 mm	70 kg·m ⁻³	Polyester and polyethylene	Silica (SiO ₂)	0.023 W·m ⁻¹ ·K ⁻¹
		5±0.5 mm				
Measured Values						
Sample	Particle diameter	Standard deviation	Fiber diameter	Standard deviation	Porosity	Extinction coefficient
CZ	10 μm±5 μm		12 μm±3 μm		91%±7%	4014 m ⁻¹
TW	13 μm±4 μm		9 μm±2 μm		79%±7%	3165 m ⁻¹

*At room temperature

Cryogel® Z

Table B-2: Measurements on 30.5 cm × 30.5 cm × 10 mm CZ using HFM (Netzsch HFM 436 Lambda) @ RH=0%, compressive load=0.5 Psi and temperature gradient= 20°C following ASTM C518

T (°C)	k (W·m ⁻¹ ·K ⁻¹)
-20	0.0147
-10	0.0148
0	0.0151
10	0.0154
20	0.0154
30	0.0157
40	0.0159
50	0.0161
60	0.0164
70	0.0164
80	0.0165

Table B-3: Measurements on 30.5 cm × 30.5 cm × 10 mm CZ using environmental chamber, ESPEC Platinous series EPX-4H and Ohaus Adventurer™ Balance following ISO 12571:2013 Standard

T (°C) @ 40% RH	Water content (%)
25	0.698
45	0.023
T (°C) @ 90% RH	Water content (%)
25	2.341
45	1.704

Table B-4: Measurements on 5 cm × 5 cm × 5 mm CZ using TPS- humidifier assembly (TPS 2500S, ThermTest Inc., Fredericton, Canada and Cellkraft F-series humidifier) with power of 10 mW, measurement time of 40 s and rest intervals of 24 hours

RH (%) @ 25°C	k (W·m ⁻¹ ·K ⁻¹)
0	0.0156
40	0.0164
80	0.0179
RH (%) @ 45°C	k (W·m ⁻¹ ·K ⁻¹)
0	0.0162
40	0.0175
80	0.0186

Table B-5: Measurements on 30.5 cm × 30.5 cm × 10 mm CZ using HFM @ 25°C and 7 mm × 7 mm × 10 mm CZ using TMA (Q400EM, TA Instruments) with a macro-expansion probe of a 6.07 mm diameter and @ 25°C

Stress (kPa) HFM	Strain (%)
0.69	0.00
1.38	5.27
2.34	8.55
3.44	11.17
4.48	13.36
6.55	17.17
7.58	19.53
7.92	20.18
Stress (kPa) TMA	Strain (%)
0.37	0.00
1.81	9.37
3.27	14.07
4.72	17.15
6.18	19.46
7.63	21.32

Table B-6: Measurements on 30.5 cm × 30.5 cm × 5 mm CZ using HFM @ 25°C and 7 mm × 7 mm × 5 mm CZ using TMA (Q400EM, TA Instruments) with a macro-expansion probe of a 6.07 mm diameter and @ 25°C

Stress (kPa) HFM	Strain (%)
0.69	0.00
1.38	3.44
2.34	7.083
3.45	9.77
4.48	11.86
Stress (kPa) TMA	Strain (%)
0.37	0.00
1.13	9.37
1.89	14.07
2.64	17.15
3.40	19.46
4.15	21.32

ThermalWrap

Table B-7: Measurements on 30.5 cm × 30.5 cm × 10 mm TW using HFM (Netzsch HFM 436 Lambda) @ RH=0%, compressive load=0.5 Psi and temperature gradient=20°C following ASTM C518

T (°C)	k (W·m ⁻¹ ·K ⁻¹)
-20	0.019
-10	0.020
0	0.020
10	0.021
20	0.022
30	0.022
40	0.023
50	0.024
60	0.025
70	0.026
80	0.027

Table B-8: Measurements on 30.5 cm × 30.5 cm × 10 mm TW using environmental chamber, ESPEC Platinous series EPX-4H and Ohaus Adventurer™ Balance following ISO 12571:2013 Standard

T (°C) @ 40% RH	Water content (%)
25	1.240
45	0.854
T (°C) @ 90% RH	Water content (%)
25	2.870
45	1.157

Table B-9: Measurements on 5 cm × 5 cm × 5 mm TW using TPS- humidifier assembly (TPS 2500S, ThermTest Inc., Fredericton, Canada and Cellkraft F-series humidifier) with power of 10 mW, measurement time of 40 s and rest intervals of 24 hours

RH (%) @ 25°C	k (W·m ⁻¹ ·K ⁻¹)
0	0.0215
40	0.0228
80	0.0238
RH (%) @ 45°C	k (W·m ⁻¹ ·K ⁻¹)
0	0.0225
40	0.0240
80	0.0252

Table B-10: Measurements on 30.5 cm × 30.5 cm × 8 mm TW using HFM @ 25°C and 7 mm × 7 mm × 8 mm TW using TMA (Q400EM, TA Instruments) with a macro-expansion probe of a 6.07 mm diameter and @ 25°C

Stress (kPa) HFM	Strain (%)
0.69	0.00
1.38	5.09
2.41	8.75
3.44	11.23
4.48	13.42
5.51	15.25
6.54	16.84
Stress (kPa) TMA	Strain (%)
0.37	0.00
1.54	0.09
2.70	0.15
3.86	0.19
5.03	0.23
6.19	0.25

Table B-11: Measurements on 30.5 cm × 30.5 cm × 5 mm TW using HFM @ 25°C and 7 mm × 7 mm × 5 mm TW using TMA (Q400EM, TA Instruments) with a macro-expansion probe of a 6.07 mm diameter and @ 25°C

Stress (kPa) HFM	Strain (%)
0.69	0.00
1.38	4.96
2.41	8.55
3.45	12.40
4.48	14.51
Stress (kPa) TMA	Strain (%)
0.35	0.00
1.21	3.50
2.08	6.66
2.95	9.06
3.82	10.98

Appendix C.

Uncertainty Analysis

Thermal conductivity/resistance, mechanical deformation, fiber and particle diameters as well as pore size of the aerogel blanket samples were measured several times, as it is explained in the thesis, and the average of the measurements for each sample was reported as the final value. The standard deviation of the reported average is obtained from following equation:

$$s = \sqrt{\frac{\sum_{i=1}^n (X_i - \bar{X})^2}{n-1}}$$

where n is the total number of measurements in sample, X is the value of measurements and sample mean can be calculated as follows:

$$\bar{X} = \frac{\sum_{i=1}^n X_i}{n}.$$

Appendix D.

Total Heat Transfer Governing Equations

The total heat transfer through an aerogel blanket includes radiation and conduction from both the gas and solid phases. By using the diffusion approximation and the radiative conductivity derived in section 2.2, the energy equation for heat transfer by combined radiation and conduction may be written as follows [25]:

$$\frac{d}{dz}[(k_{rad.} + k_{cond.})] = 0 \quad (D-1)$$

Total heat flux between two boundaries with different emittance (ε_1 and ε_2) and temperatures can be defined as follows

$$q_{tot} = (1/C_0) \{ \sigma(T_1^4 - T_2^4) + (3\tau_0 / 4t_s) k_{cond.} (T_1 - T_2) \} \quad (D-2)$$

where

$$C_0 = \frac{3\tau_0}{4} + \left(\frac{1}{\varepsilon_1} - \frac{1}{2} \right) \left[\frac{1}{1 + k_{cond.} / k_{rad.}(T_1)} \right] + \left(\frac{1}{\varepsilon_2} - \frac{1}{2} \right) \left[\frac{1}{1 + k_{cond.} / k_{rad.}(T_2)} \right] \quad (D-3)$$

and τ_0 is the optical thickness ($K_R \times t_s$).

An effective total thermal conductivity can be defined based on the total heat flux given by Eq. (D-2) and the temperature gradient across the thickness of the sample:

$$k_{eff.} = \frac{q_{tot} \times t_s}{(T_1 - T_2)} \quad (D-4)$$

Having the limit of large optical thickness in aerogel blankets, the same emittance for both boundaries and negligible temperature gradient, Eq. (D-4) reduces to

$$k_{eff.} = k_{cond.} + \frac{16\sigma T^3}{3K_R} = k_{cond.} + k_{rad.} \quad (D-5)$$

Indicating that heat transfer by radiation and conduction are additive for optically thick media.